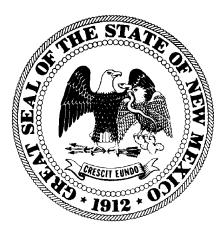
# State of New Mexico Continuing Planning Process

# (Appendix A)



# Antidegradation Policy Implementation Procedure

Adopted by the New Mexico Water Quality Control Commission [insert date of adoption]

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- **1** ANTIDEGRADATION POLICY IMPLEMENTATION PROCEDURES
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#### I. INTRODUCTION

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6 The Antidegradation Implementation Procedures (Procedures) establish the 7 process for implementing the Antidegradation Policy (Policy) in the *Standards for* 8 *Interstate and Intrastate Surface Waters* (New Mexico Water Quality Standards), 9 20.6.4.8 NMAC. The Procedures should be construed in conjunction with other 10 planning tools approved by the Water Quality Control Commission, including the 11 Integrated Clean Water Act (CWA) Section 303(d)/305(b) List and Report, and the 12 Statewide Water Quality Management Plan.

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#### 14 **II. TIER DEFINITIONS**

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16 The Policy establishes three categories of waters. These categories are called 17 "tiers". The tier designation requires different levels of review and allows different levels 18 of degradation. Tier 1 and 2 designations are made on a parameter-by-parameter 19 basis. As a result, a water may be Tier 1 for one parameter and Tier 2 for a different 20 one. Tier 3 designation is made based on the special nature of the water.

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Figure 1 illustrates the tier designation process.

- 24 **A. Tier 1**
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Tier 1 applies to waters that do not meet or meet but are not better than the 26 water quality standards for existing or designated uses.<sup>1</sup> Tier 1 waters that require Tier 27 1 review will be identified by assessing water quality information pursuant to established 28 29 protocols. Waters identified as "impaired" for any existing or designated use according to the current State of New Mexico Procedures for Assessing Standards Attainment for 30 the Integrated §303(d) / §305(b) Water Quality Monitoring and Assessment Report: 31 Assessment Protocol<sup>2</sup> automatically will be Tier 1 for the parameter of concern. Waters 32 not identified as impaired on New Mexico's Integrated CWA 303(d) / 305(b) List will be 33 evaluated on a case-by-case basis. The Department will conduct the evaluation using 34

<sup>&</sup>lt;sup>1</sup> The terms "existing use" and "designated use" are defined in the *Code of Federal Regulations* (40 CFR 131.3) and the New Mexico Water Quality Standards (20.6.4.7 NMAC). The terms are not interchangeable and are subject to different levels of protection depending on the specific use. *See, e.g.,* 

<sup>40</sup> CFR 131.10.

<sup>&</sup>lt;sup>2</sup> The protocol is based in part upon USEPA's *2002 Integrated Water Quality Monitoring and Assessment Report Guidance*; 2001 Memorandum from Robert H. Wayland, Office of Wetlands, Oceans, and Watersheds. Washington D.C.

the available water quality information and the same protocols used to develop the
 Integrated 303(d) / 305(b) report.

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The Policy defines the level of protection for Tier 1 waters: "Existing instream water uses and the level of water quality necessary to protect the existing uses shall be maintained and protected." 20.6.4.8.A.1 NMAC. Existing uses are uses "actually attained in a surface water on or after November 28, 1975, whether or not they are actually included in the water quality standards." See 40 CFR 131.3(e); 20.6.4.6.Q NMAC. Tier 1 defines the minimum level of protection afforded to all waters regardless of tier designation.

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#### B. Tier 2

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Tier 2 applies to waters whose quality is better than necessary to protect the CWA Section 101(a)(2) goals. Tier 2 applies to all classified waters (e.g., identified in the New Mexico Water Quality Standards, Sections101 through 899) that are not designated as Tier 1 on a parameter-by-parameter basis or as Tier 3. Tier 2 may apply to unclassified waters on a parameter-by-parameter basis depending on the available water quality information. Like Tier 1 waters, Tier 2 waters will be identified by assessing water quality information pursuant to established protocols.

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The Policy defines the level of protection for Tier 2 waters:

24 Where the quality of a surface water of the state exceeds levels 25 necessary to support the propagation of fish, shellfish, and wildlife, 26 and recreation in and on the water, that quality shall be maintained and protected unless the commission finds,<sup>3</sup> after full satisfaction of 27 the intergovernmental coordination and public participation 28 29 provisions of the state's continuing planning process, that allowing 30 lower water quality is necessary to accommodate important economic and social development in the area in which the water is 31 32 located. In allowing such degradation or lower water quality, the state shall assure water quality adequate to protect existing uses 33 34 fully. Further, the state shall assure that there shall be achieved the highest statutory and regulatory requirements for all new and 35 existing point sources and all cost-effective and reasonable BMPs 36 for nonpoint source control. Additionally, the state shall encourage 37 38 the use of watershed planning as a further means to protect surface 39 waters of the state.

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20.6.4.8.A.2 NMAC.

<sup>&</sup>lt;sup>3</sup> Pursuant to the New Mexico Water Quality Act, Section 74-6-4.E, the Commission delegated responsibility for implementing the antidegradation policy to the Department. *See* 20.6.4.8.E NMAC.

1 In Tier 2 waters, limited degradation may be allowed after consideration of 2 several factors, including:

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- the discharge's potential to affect existing or designated uses or to interfere with CWA Section 101(a)(2) goals (water quality which provides for the "protection and propagation of fish, shellfish, and wildlife and provides for recreation in and on the water");<sup>4</sup>
- 2) the need to accommodate important economic and social development in the area in which the water is located; and
- 3) the availability of discharge alternatives, including no discharge, reuse, land disposal, pollution prevention or reduction, and pollutant trading with point and non-point sources.
- 17 Even if the decision is made to allow degradation in Tier 2 waters, water quality must be maintained to ensure the protection of existing uses. Water quality also must 18 be maintained to ensure the protection of designated uses unless the designated uses 19 are modified through a use attainability analysis, 40 CFR 131.10(j) and 20.6.4.14 20 NMAC, or adequately protected by segment-specific water quality standards. Finally, 21 22 water quality must be maintained to ensure the protection of the CWA Section 101(a)(2) uses. The applicant for the new or increased discharge (or an existing discharge in 23 certain circumstances as described on page 7) bears the burden of demonstrating the 24 25 social and economic need for degrading water quality.
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27 **C. Tier 3** 

29 The Policy defines the level of protection for Tier 3 waters:

No degradation shall be allowed in high quality waters designated by the commission as outstanding national resource waters (ONRWs). ONRWs may include, but are not limited to, surface waters of the state within national and state monument, parks, wildlife refuges, waters of exceptional recreational or ecological significance, and waters identified under the Wild and Scenic Rivers Act.

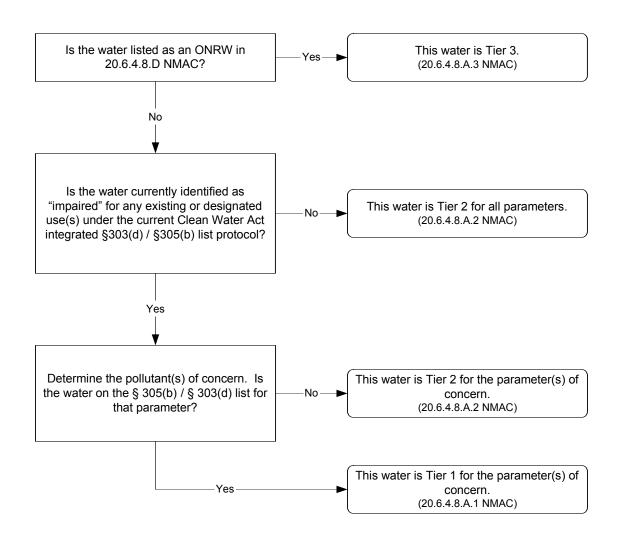
Tier 3 applies to waters that are designated by the Commission as "outstanding national resource waters." The Commission designates Tier 3 waters after public notice and comment pursuant to procedures established in the New Mexico Water Quality Standards. *See* 20.6.4.8.B NMAC.

<sup>&</sup>lt;sup>4</sup> Commonly referred to as the "fishable/swimmable goals".

1 The Policy prohibits any degradation in Tier 3 waters. 20.6.4.8.A.3 NMAC. 2 However, this prohibition does not mean that all discharges are prohibited. In special 3 circumstances, a discharge may be allowed if it does not cause degradation or causes 4 only temporary and short-term changes in water quality that do not impair existing uses 5 or if the activity is intended to implement the §101(a) objectives of the CWA. Such 6 special circumstances must undergo antidegradation review.

#### Figure 1. Tier Determination Flowchart

(Flow chart summarizes preceding narrative description, refer to narrative for complete detail)



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#### III. IMPLEMENTATION

3 The Procedures apply to every proposal for a new or increased discharge of a pollutant to a "surface water of the State."<sup>5</sup> "New or increased discharge" includes 4 NPDES permits issued by the USEPA pursuant to CWA Section 402 and Dredge-and-5 Fill Permits issued by the U.S. Army Corps of Engineers (Army Corps) pursuant to CWA 6 7 Section 404. The Procedures also apply to the renewal of permits for existing 8 discharges in certain circumstances as determined by the Department, including a 9 single discharge causing degradation over time, a single source contributing to 10 cumulative degradation, and a single source with a history of permit noncompliance. The Procedures do not apply to other water quality-related actions, including revision of 11 Commission documents (e.g., New Mexico Water Quality Standards, Continuing 12 13 Planning Process, Water Quality Management Plan, and Nonpoint Source Management Program), the Commission's establishment of Total Maximum Daily Loads (TMDLs), or 14 the conduct of studies, including use attainability analyses, by any party, including the 15 Department.<sup>6</sup> These types of water guality-related actions already are subject to 16 extensive requirements for review and public participation, as well as various limitations 17 on degradation imposed by state and federal law. 18 19

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### 1. Tier 1

23 24 The Department employs the CWA Section 401 certification process to ensure that water quality that does not meet or that meets but is not better than the water 25 26 quality standards for existing uses in Tier 1 waters is not degraded by a new or 27 increased discharge or the renewal of a permit for an existing discharge. See Continuing Planning Process - Process for the Development of Effluent Limitations. 28 29 Section 401 certification ensures that NPDES and Dredge-or-Fill permits are consistent with state law, protect the water quality standards, and implement the water quality 30 management plan, including TMDLs. Section 401 certification also ensures that 31 NPDES permits comply with the federal requirement that a new or increased discharge 32 will not cause or contribute to a violation of water quality standards, unless such 33 discharge is authorized by a TMDL waste load allocation or similar mechanism prior to 34 35 TMDL establishment. See 40 CFR 122.4(i).<sup>7</sup> 36

A. POINT AND REGULATED SOURCES

<sup>&</sup>lt;sup>5</sup>The term "surface water of the State" is defined in the New Mexico Water Quality Standards, 20.6.4.7.RR NMAC.

<sup>&</sup>lt;sup>6</sup> See Section 4.8, *Water Quality Standards Handbook* (USEPA 1994).

<sup>&</sup>lt;sup>7</sup>There is no comparable federal requirement for Dredge-or-Fill Permits, but the Department uses Section 401 certification to ensure that a new or increased discharge complies with TMDL waste load allocations.

There are a number of opportunities for public participation in the review of new and increased discharges into Tier 1 waters. The Commission adopts TMDLs for Tier 1 waters not meeting water quality objectives. This process includes public notice and comment. The USEPA and Army Corps follow detailed procedures requiring public notice and comment when issuing NPDES and Dredge-or-Fill permits. Finally, the Department's Section 401 certification can be appealed and a full hearing held before the Commission.

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#### 2. Tier 2

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#### a. Determination of Necessity

13 Tier 2 screening is triggered when a new or increased discharge or the renewal 14 of a permit for an existing discharge is proposed for a receiving water with existing water quality better than necessary to support the propagation of fish, shellfish, and 15 wildlife, or recreation in and on the water. The initial focus is the magnitude of the effect 16 17 on water quality. If the magnitude of the effect on water quality exceeds a specified level, Tier 2 review will be conducted. Below that specified level, Tier 2 review will not 18 19 be conducted. By establishing a *de minimis* level above which Tier 2 review will be conducted, limited state resources are directed to new or increased discharges and the 20 renewal of permits for existing discharges with the likelihood of causing significant 21 22 degradation of water quality. Establishing *de minimis* action levels also helps reduce 23 overall costs for the Department the general public and dischargers.

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25 In rare instances the WQCC may consider either establishing or revising a TMDL - Waste Load Allocation (WLA) in a Tier 2 water. This situation might arise where a 26 previously established TMDL for a former Tier 1 water has been successful in restoring 27 water quality and there is a subsequent application to revise the TMDL-WLA to allow an 28 increase in the discharge of pollutants. In this situation two processes come into 29 30 consideration, the public and commission review of the TMDL and the Department's review of the TMDL under the antidegradation policy. When this situation occurs, the 31 two processes may for efficiency be held simultaneously or sequentially depending on 32 33 the specific circumstances of the case.

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The Department will evaluate whether the magnitude of the effect on water 35 36 quality exceeds a specific level on a parameter-by-parameter basis. The evaluation will be conducted using numeric criteria only, because of the impracticability of applying the 37 process to narrative criteria. It should be noted that the decision to use numeric criteria 38 39 does not expose Tier 2 waters to substantial degradation of water quality because these waters are protected by overlapping designated and existing uses and their associated 40 criteria, as well as by the NPDES and Dredge-or-Fill permits and Section 401 41 42 certification which must be written to protect the narrative criteria.

Figure 2 illustrates the process for determining whether a new or increased 1 discharge is subject to Tier 2 review. The following text explains the figure in more 2 3 detail.

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#### Publicly Owned and Private Domestic Treatment Work i) Discharges

8 For purpose of Tier 2 review, the following new or increased discharges and the 9 renewal of permits for existing discharges by publicly owned treatment works (POTWs) and privately owned domestic treatment works (PODTWs) are considered de minimis 10 and are not subject to Tier 2 review provided that the assimilative capacity is more than 11 10% of the criterion for the parameter of concern and: 12

- 14 1) the POTW or PODTW has a design capacity of 0.1 million gallons per day or less and is eligible to omit Part B of the NPDES permit application 15 form (OMB Number 2040-0086, Approved 1/14/99);<sup>8</sup> 16
- 17 2) the design capacity of the POTW or PODTW or the pollutant load 18 19 (measured on a parameter-by-parameter basis) will increase 10 percent 20 or less in a five-year period, and the exemption is not used for two 21 consecutive permits;
- 23 3) the design capacity of the POTW or PODTW will increase by 10 to 25 percent in a five-year period, the POTW or PODTW demonstrates to the 24 Department's satisfaction that it is implementing a water conservation or 25 26 wastewater reuse or diversion program designed to reduce the discharge volume by at least 10 percent in that five-year period, and the exemption 27 is not used for two consecutive permits; 28 29
- 30 4) the design capacity of the POTW or PODTW is 10 percent or less of the critical low flow of the receiving stream (as defined in the water quality 31 32 standards);
- 5) the POTW or PODTW demonstrates to the Department's satisfaction that its pollutant load (measured on a parameter-by-parameter basis) will 35 be offset by enforceable reductions by other point or nonpoint sources within the same waterbody segment as the new or increased discharge; or
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<sup>&</sup>lt;sup>8</sup> During the development of the revised NPDES permit application form, USEPA studied the potential for minor POTWs and PODTWs to cause violations of water quality standards. USEPA found that these facilities posed an extremely low probability of causing a violation of water quality standards because of their low volume and effluent quality (even without considering the ameliorative effect of dilution). 64 Fed. Reg. 42433 (August 4, 1999).

6) the new or increased discharge or the renewal of a permit for an existing discharge was reviewed in an Environmental Assessment (EA) or Environmental Impact Statement (EIS) that considered water quality impacts and the social and economic development in the area in which the water is located and that was conducted in accordance with federal regulations, and in the case of an EA, the responsible federal agency made a Finding of No Significant Impact (FONSI).

9 Notwithstanding these *de minimis* activities, the Department shall conduct Tier 2 10 review for any new or increased discharge or the renewal of a permit for an existing 11 discharge by a POTW or PODTW when the discharge, taken together with all other 12 activities allowed after the baseline water quality is established<sup>9</sup>, would cause a 13 reduction in the available assimilative capacity of 10 percent or more for the parameter 14 of concern.

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For purpose of this section, available assimilative capacity is defined as the difference between the baseline water quality and the water quality criterion for the parameter of concern. (See Appendix C to this document for guidelines for calculating assimilative capacity).

Figure 2 illustrates the process for determining whether a new or increased discharge or the renewal of a permit for an existing discharge by a POTW or PODTW is subject to Tier 2 review. Figure 2 is presented for illustration only and may not address all possible circumstances. In the event of omission, ambiguity or conflict, the written provisions of these procedures will control.

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#### ii) Industrial Discharges

For purpose of Tier 2 review, the following new or increased discharges and the renewal of permits for existing discharges by industrial activities are considered *de minimis* and are not subject to Tier 2 review provided that the assimilative capacity is more than 10% of the criterion for the parameter of concern and:

1) the discharger demonstrates to the Department's satisfaction that the new or increased discharge will consume 10 percent or less of the available assimilative capacity for the pollutant of concern;

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2) the discharger demonstrates to the Department's satisfaction that its pollutant load (measured on a parameter-by-parameter basis) will be offset by enforceable reductions by other point or nonpoint sources within the same waterbody segment as the new discharge; or

<sup>&</sup>lt;sup>9</sup> When evaluating the "baseline" condition, the Department will consider any previous antidegradation reviews for the same body of water to prevent cumulative impacts.

3) the new or increased discharge or the renewal of a permit for an existing discharge was reviewed in an EA or EIS that considered water quality impacts and the social and economic development in the area in which the water is located and that was conducted in accordance with federal regulations, and in the case of an EA, the responsible federal agency made a FONSI.

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9 Notwithstanding these *de minimis* activities, the Department shall conduct Tier 2 10 review for any new or increased discharge or the renewal of a permit for an existing 11 discharge by an industrial activity when the discharge, taken together with all other 12 activities allowed after the baseline water quality is established, would cause a 13 reduction in the available assimilative capacity of 10 percent or more for the parameter 14 of concern.

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For purpose of this section, available assimilative capacity is defined as the difference between the baseline water quality and the water quality criterion for the parameter of concern. (See Appendix C to this document for guidelines for calculating assimilative capacity).

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#### iii) General Permits

New or increased discharges and the renewal of permits for existing discharges covered by NPDES General permits and Dredge-or-Fill Nationwide and Regional permits present special considerations regarding Tier 2 review because of their approach of authorizing categories of discharges over a broad geographic range. Three categories of NPDES General permits (No Discharge, Storm water, and Aquifer Remediation) and several categories of Nationwide (Dredge-or-Fill) permits have been issued in New Mexico.

EPA has not issued any national guidance regarding Tier 2 review for general permits. Accordingly, the Commission adopts the following approach for general permits in New Mexico. Further, the Department reserves the right to require that any new or increased discharge or the renewal of a permit for an existing discharge (1) be subject to Tier 2 review if warranted by the facts and circumstances, or (2) be required to obtain an individual NPDES or Dredge-or-Fill permit (and thereby subject to Tier 2 review).<sup>10</sup>

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#### a) No Discharge General Permits

<sup>&</sup>lt;sup>10</sup> Federal regulations for NPDES General Permits (40 CFR 122.28) and Dredge-and-Fill Nationwide and Regional Permits (33 CFR 325.7) require a discharger to obtain an individual NPDES or Dredge-and-Fill permit if, *inter alia*, circumstances have changed since the original authorization or the discharge is deemed to be "significant".

Existing and former "No Discharge General Permits" include NPDES General Permits for Oil and Gas Facilities in the Onshore Subcategory of the Oil and Gas Extraction Point Source Category (Onshore O&G)<sup>11</sup> and Concentrated Animal Feeding Operations (CAFOs).

The Onshore O&G NPDES General Permit prohibited all discharges of pollutants to waters of the United States. 56 Fed. Reg. 7698 (February 25, 1991). Because discharges covered by this general permit were prohibited, water quality would not be degraded. In addition, Onshore O&G activities generally are considered to have social and economic importance to New Mexico.

The CAFO General Permit prohibits all discharges unless caused by (1) a storm event greater than the 25-year 24-hour storm for the CAFO location; (2) chronic rainfall greater than the 25-year 24-hour storm for the CAFO location; or (3) a catastrophic event, such as a tornado, provided that the CAFO is properly designed and operated. 58 Fed. Reg. 7611 (February 8, 1993). Because discharges covered by this general permit are prohibited except in exceptional circumstances beyond the control of the CAFOs, the degradation of water quality, beyond temporary or short-term impacts, is unlikely. In addition, CAFOs - primarily dairies and cattle feedlots - generally are considered to have social and economic importance to New Mexico.

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#### b) Storm Water General Permits

29 Storm Water General Permits include the NPDES General 30 Permits for Storm Water Discharges from Construction Activities, 68 Fed. Reg. 39087 (July 1, 2003), and the NPDES General Permit for 31 32 Storm Water from Industrial Activities, 65 Fed. Reg. 64746 (October 30, 2000). Storm water discharges are transient in nature, particularly in the 33 34 desert climate of New Mexico. Storm water discharges from construction activities are even more transient because they occur only 35 during the construction itself. Further, storm water dischargers seeking 36 coverage under these general permits are required to identify pollutants 37 38 on a parameter-by-parameter basis and to design and implement 39 controls to prevent or reduce their discharge. As a result, storm water 40 discharges that comply with general permits are not likely to cause significant degradation of water quality. In addition, industrial and 41

<sup>&</sup>lt;sup>11</sup> The oil & gas permit expired on February 25, 1996. As of August 2004, EPA has no plan to reissue the permit. It is included in this discussion as an example of the types of general permits that have occurred in NM and therefore may occur in the future.

construction activities generally are considered to have social and economic importance to New Mexico.

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#### c) Aquifer Remediation General Permits

7 The Aguifer Remediation General Permit was the NPDES General Permit for Discharges Resulting from Implementing Corrective 8 9 Action Plans for Cleanup of Petroleum UST Systems. 62 Fed. Reg. 61116 (November 14, 1997). These discharges resulted from projects 10 implemented to remediate groundwater contaminated with petroleum 11 products from leaking underground storage tanks. The general permit 12 imposed stringent effluent limitations on these discharges, even though 13 they are considered to be relatively clean. Accordingly, these kinds of 14 discharges are not expected to cause degradation to water quality. 15 Moreover, because 90 percent of New Mexico's population relies on 16 groundwater for drinking water (2000 CWA § 305(b) Report, page 87), 17 these discharges are considered to have social and economic 18 19 importance to New Mexico.

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#### d) Dredge or Fill General Permits

23 The Dredge-or-Fill General Permit authorizes the discharge of fill material within the ordinary high water mark of waters of the United 24 States. The Army Corps under CWA Section 404 regulates these 25 The Department, pursuant to its CWA Section 401 26 discharges. certification of this general or "Nationwide" permit, requires dischargers 27 to obtain specific authorization before commencing the discharge. As a 28 result, dischargers are subject to Section 401 certification review. 29 Based on this review, the Department may grant the authorization, grant 30 the authorization with conditions, or deny the authorization. 31 32 implement the Policy, the Department will use the authorization process to evaluate whether a discharge will cause significant degradation of 33 A discharge will be deemed to cause significant 34 water quality. degradation of water quality if the load of pollutants is quantifiable<sup>12</sup> and 35

<sup>&</sup>lt;sup>12</sup> Pollutant loads from Dredge or Fill permits are often difficult or impossible to quantify in the same manner as practiced in NPDES permits. Dredge or Fill permits are often temporary construction measures in or near a watercourse that may result in disturbance or deposition of sediments in the water. The primary tool for limiting the discharge of pollutants (e.g., sediment and contaminated sediment) from these activities is through permit requirements mandating the installation and operation of best management practices (BMPs) that prevent pollutant transport to a watercourse and thereby degradation. The SWQB reviews dredge or fill projects pursuant to conditions of the State's CWA Section 401 certification of the Nationwide permits. The SWQB has long employed a strategy of requiring the implementation of BMPs, necessary to protect state water quality standards that are designed to prevent [footnote continued on next page]

(1) the new or increased discharge or the renewal of a permit for an 1 existing discharge will consume 10 percent or more of the total 2 assimilative capacity for the pollutant of concern, or (2) the new or 3 4 increased discharge or the renewal of a permit for an existing discharge, 5 taken together with all other activities allowed after the baseline water quality is established, would cause a reduction in the available 6 7 assimilative capacity of 10 percent or more for the parameter of 8 concern.

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10 For purpose of this section, available assimilative capacity is defined as the 11 difference between the baseline water quality and the water quality criterion for the 12 parameter of concern.

If the Department determines that a discharge will cause significant degradation,
 the Department will either impose conditions to avoid significant degradation or require
 Tier 2 review.

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#### e) Future General Permits

General permits are an important tool in addressing categories of discharges where large numbers of facilities are engaged in similar activities such as those described above. Review of future proposed general permits will be on a case-by-case basis. The Department will consider the nature of the permit requirements and determine a course of action.

As practical guidance:

- 1. No Discharge general permits such as the no discharge CAFO and Oil &
   Gas cited above may be considered *de minimis* impacts and may not be
   required to proceed through full Tier 2 antidegradation review. The
   Department may at its discretion initiate a review if it deems the case-by case circumstances warrant such action;
  - 2. Storm water general permits for industrial activities such as those cited above may be considered *de minimis* and may not be required to proceed through full Tier 2 antidegradation review. The Department may at its discretion initiate a review if it deems the case-by-case circumstances warrant such action;
- 373. Storm water general permits for municipal or urban runoff may be38proposed to comply with CWA Section 402(p). Urban runoff from39municipalities has existed historically but has not been regulated under40the NPDES program. Consideration should be given that these41discharges may be from existing systems and as such are existing42discharges. New permit requirements such as implementation of best

to maximum extent possible the discharge of pollutants instead of allowing a particular quantity of pollutant to be discharge.

management practices will reduce existing loads of pollutants entering the storm sewer system and therefore the receiving water. Therefore these permit actions should be considered as reducing any degradation that may result from these discharges and therefore not require Tier 2 antidegradation review.

- 4. Environmental remediation permits such as the aquifer remediation general permit cited above may be considered *de minimis* impacts and in the public interest for social and economic benefit and may not be required to proceed through full Tier 2 antidegradation review. The Department may at its discretion initiate a review if it deems the case-bycase circumstances warrant such action;
  - 5. Dredge or Fill Permits General Permits (or Nationwide Permits) should continue to be reviewed in the same manner as existing Dredge or Fill permits. The Department may at its discretion initiate a review if it deems the case-by-case circumstances warrant such action;
- The Department should consider other types of general permits on a case-by-case basis with the same principles as considered in the above examples. The Department shall advise the Commission of *de minimis* determinations in respect to general permit certifications at the first WQCC meeting after the permit certification is completed.
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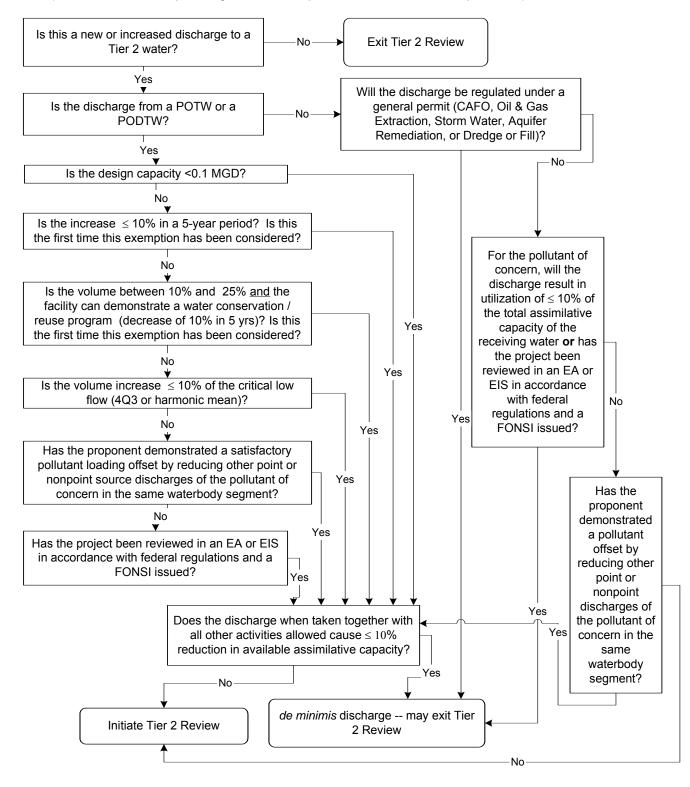
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#### Figure 2. Tier 2 Review - Eligibility Flowchart (Flow chart summarizes preceding narrative description, refer to narrative for complete detail)



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2		b. Conducting Tier 2 Review
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9		i) Information Gathering
10 11 12 13 14 15 16 17 18 19 20 21 22 23	notify the ap or the rene information require to c the applica applicant's adequate a satisfaction determine t applicant's	in 30 days of receipt of the complete permit application, the Department shall oplicant regarding the standard of review for the new or increased discharge eval of a permit for an existing discharge and its obligation to submit the described below, as well as any other information that the Department may onduct the review. Within 30 days of receipt of the Department's notification, nt shall submit the required information. Within 30 days of receipt of the response, the Department shall notify the applicant whether the response is and whether additional information is required. Upon the applicant's of the Department's requests for information, the Department shall hat the application is complete and initiate the antidegradation review. The failure to submit the requested information may result in certification denial permit issuance.
24 25	The	Department shall request at least the following information:
26 27 28 29	area	inalysis of important social or economic activities and development in the in which the water is located that may be <i>beneficially</i> impacted by the new creased discharge or the renewal of a permit for an existing discharge;
30 31 32 33	area	inalysis of important social or economic activities and development in the in which the water is located that may be <i>adversely</i> impacted by the new or eased discharge or the renewal of a permit for an existing discharge;
34 35	3) An a	nalysis of the following factors, quantified to the greatest extent possible;
36 37	a)	employment;
37 38 39	b)	production of goods and services;
39 40 41	c)	tax base;
41 42 43	d)	housing;
43 44	e)	effect on existing or expected environmental and public health problems;

1		
1 2	f)	any other relevant information; and
3	• /	
4 5 6 7	water	nalysis of alternative disposal options (including no discharge to a surface) or discharge reduction options, including any option that would minimize dation.
8 9 10 11	•	partment also may require, in its discretion, that the applicant the Antidegradation Data Worksheets in Appendix A or Appendix
12		ii) Preliminary Decision-Making
12		
13 14 15 16 17 18 19	pursuant to decision to c	n 60 days of the Department's determination that the information submitted the above paragraph is complete, the Department shall make a preliminary deny or authorize the degradation. The Department shall prepare a written f basis for the preliminary decision containing the following information (as
20	a)	Applicant's name, facility, and location;
21		
22 23 24	b)	Description of the discharge, including the nature and concentration of pollutants;
25 26 27	C)	Description of receiving water, existing and designated uses, and applicable criteria;
28 29 30	d)	Identification of the permit and the facility's permitting and enforcement history;
31 32 33 34	e)	Description of treatment or best management practices to be employed and a brief description of alternative disposal options evaluated by the applicant.
35 36 37	f)	Estimation of the amount of requested degradation and impact on receiving water and existing and designated uses;
38 39 40	g)	Analysis of economic or social importance and whether and what magnitude of degradation is necessary to accommodate it;
41 42 43	h)	Description and brief discussion of conditions to be imposed upon discharge; and
43 44 45	j)	Description of the procedures for reaching a final decision including:

1	1) The comment period and address where comments may be sent;
2 3 4	2) Procedure for obtaining a public hearing;
4 5 6	3) Other procedures for public participation in the final decision;
0 7 8	4) Departmental contact for additional information.
9	iii) Public Comment and Intergovernmental Coordination
10 11 12 13 14 15 16 17 18 19 20	The Department will publish notice and provide an opportunity to comment on the preliminary decision and statement of basis. The public comment period shall be no less than 30 days. During the public comment period, any interested person may submit written comments and request a public hearing. A request for a public hearing must be in writing and must state the nature of the issues to be raised. If the Department determines that the request for public hearing raises issues of significant public interest within the scope of the antidegradation policy, the Department will hold a public hearing. The public hearing will be held in a location near the water affected by the discharge.
20 21 22	With respect to the public notice, the Department shall:
22 23 24	1) Publish legal notice in a newspaper of general circulation in the affected area;
25 26	2) Post the legal notice on the Department website;
27 28 29	3 Mail the legal notice to all persons who have submitted a written request to the Commission for advance notice of preliminary decisions and provided the Commission with a mailing address; and
30 31 32 33	<ol> <li>The legal notice shall describe where a copy of the preliminary decision and statement of basis may be obtained.</li> </ol>
34	iv) Final Decision
35 36 37 38 39 40 41 42 43 44	<ul> <li>Within 60 days after the later of the close of the public comment period or the public hearing, the Department shall issue a final decision and a written statement of basis. The statement of basis shall:</li> <li>1) Review the relevant facts, including the applicant, facility, water, uses, and criteria;</li> <li>2) Identify changes from the preliminary decision and statement of basis;</li> </ul>

- 3) Identify and summarize the basis for any conditions to be imposed on the discharge, including citations to applicable statutory and regulatory provisions;
- Respond to comments on the preliminary decision and statement of basis, including comments during the public comment period and public hearing, if any; and
- 5) Describe the process for filing an appeal with the Commission.

10 The Department shall send the final decision to the applicant and to each person 11 who submitted written comments or requested notice of the final decision. The final 12 decision shall be effective immediately.

13

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- 3. Tier 3
- 14 15

The Policy prohibits the degradation of Tier 3 waters by a new or increased 16 discharge or the renewal of a permit for an existing discharge, but this prohibition is not 17 the same as prohibiting any new or increased discharge or the renewal of a permit for 18 19 an existing discharge. It is theoretically possible for an applicant to make a case-bycase demonstration that a new or increased discharge or the renewal of a permit for an 20 21 existing discharge will not cause degradation or will cause only temporary and shortterm changes in water quality that do not impair existing uses. Any application for a 22 new or increased discharge or the renewal of a permit for an existing discharge in a Tier 23 3 water will be considered on a case-by-case basis applying the Tier 2 review process 24 as modified by the Department to reflect unique factors associated with the Tier 3 water. 25 26 The unique factors should include the specific goal and the environmental impact of 27 these activities, and the intensity and duration of those impacts and how the impacts will be minimized. 28

- 29
- 30

#### **B. NONPOINT SOURCES**

31

32 Federal law does not require the Commission to apply the Policy to nonpoint sources. American Wildlands v. Browner, 260 F.3d 1192 (10th Cir. 2001); 40 CFR 33 131.12(a)(2) (encouraging but not mandating enforceable controls on nonpoint 34 35 sources). The Water Quality Standards Implementation Plan "... encourages, in conjunction with other state agencies, voluntary implementation of the best 36 management practices set forth in the New Mexico statewide water quality management 37 plan and the nonpoint source management program." 20.6.4.8.E(13) NMAC. The New 38 Mexico Nonpoint Source Management Program<sup>13</sup> also ... uses a voluntary approach to 39

<sup>&</sup>lt;sup>13</sup> New Mexico Nonpoint Source (NPS) Management Program. 1999. Executive summary page viii. The program was approved by USEPA January 6, 2000. The NPS Management Program is incorporated by reference in the *Statewide Water Quality Management Plan* (Work Element 4).

1 achieve water quality improvements." Accordingly, the Policy does not apply to 2 nonpoint sources.

3

4 Although the Policy does not apply to nonpoint sources, the Commission 5 implements a straightforward approach to address degradation of water quality by nonpoint sources. First, the Commission adopted the Water Quality Management Plan, 6 which requires TMDLs for waters affected by nonpoint source pollution that contain Best 7 Management Practices (BMPs). Second, the Commission adopted the Nonpoint 8 Source Management Program, which awards Section 319(h) funds for persons to 9 10 implement those BMPs. See Section VII - Impaired Waters Identification and Abatement Strategy. 11

12

#### 13 IV. APPEALS

14

15 Persons adversely affected by any final decision of the Department may appeal 16 to the Commission in accordance with the New Mexico Water Quality Act.

### APPENDIX – A Tier 2 Review of a Public Facility

Appendix A includes additional information that may be required by the Department to evaluate socio-economic factors of a public facility during a Tier 2 review. This evaluation is based on two types of impacts, referred to as "substantial" and "widespread". The Substantial Impacts analysis is found in Tables A-3 – A-7. The Widespread Impacts<sup>14</sup> analysis is found in Table A-8.

8

#### 9 SUBSTANTIAL IMPACTS - SUMMARY

10

Purpose of Substantial Impacts analysis: Determine whether a public facility can
 afford pollution controls in order to avoid any degradation of water quality.

13

The first step in a Substantial Impacts analysis is to provide data on the socio-economic factors listed in the worksheets in Tables A-1 and A-2. This data is then used to determine two indicators called the "Municipal Affordability Screener" (Table A-3) and the "Secondary Affordability Test" (Tables A-4 – A-6). The results of these indicators are then compared in the "Assessment of Substantial Impacts Matrix" (Table A-7) as a way to determine overall affordability to the community.

20

### 21 Widespread Impacts - Summary22

Purpose of widespread impacts analysis: Evaluates the social costs of pollution control
 requirements by: 1) Defining the affected community; 2) Evaluating the community's
 current characteristics; and 3) Evaluating how community characteristics would change
 if discharger must avoid degradation to water quality.

27

If the conclusion from the Substantial Impacts analysis is "Questionable Affordability" or "Community cannot afford the pollution control", then a Widespread Impacts analysis may be completed to further resolve the affordability issue. This analysis is primarily a qualitative evaluation based on community socioeconomic factors that are expanded to a larger scale than the Substantial Impacts analysis.

<sup>&</sup>lt;sup>14</sup> Widespread Impact Analysis forms derived from EPA's Water Quality Standards Academy Participant Manual Update-4, 2000 [EPA 823-B-00-005].

2

#### Table A-1. Antidegradation Data Worksheet

SOCIO-ECONOMIC INDICATORS	DATA
CITY'S DEMOGRAPHICS	
Population(year)	
Current Population(year)	
Type of household moving away from (city)	
Number of households	
Median Household Income (U.S. Census, Census Designated Place)	
Median Household Income (Local Planning Board Estimates, City)	
Median Household Income (U.S. Census, State)	
Median Household Income (U.S. Census, County)	
Major Type of Employment	
Regional Economic Conditions	
% of Total Wastewater Flow from Residential & Municipal Sources	
Unemployment Rate (City)	
Unemployment Rate (County)	
Unemployment Rate (State)	
CITY'S FINANCIAL HISTORY	
Property Tax Revenues(year)	
Sales Tax & Miscellaneous Revenues(year)	
Total Government Revenues(year)	
Property Tax Revenues (FY)	
Sales Tax & Miscellaneous Revenues (FY)	

Total Government Revenues (FY)	
Current Market Value of Taxable Property (FY)	
Property Tax Delinquency Rate	
Bond Rating - insured sewer	
Bond Rating - non insured sewer	
Overall Net Debt (FY)	

3

### Table A-2. Antidegradation Data Worksheet

	SOCIO-EC	DATA				
	tment Options ( of Water Qualit	(pollution controls) that will Avoid				
Capital Impro	vements					
OPTION 1.	(year)	dollars				
OPTION 2.	(year)	dollars				
Annual Opera	ating Costs					
OPTION 1.	(year)	dollars				
OPTION 2.	(year)	dollars				
FINANCING	FOR WASTEW	ATER TREATMENT OPTIONS				
OPTION 1. S	ource of Financi	ng				
Repayment T	erm, Vehicle					
Bond Rate						
Total Annual	Total Annual Cost of Existing Plant					
OPTION 2. S	ource of Financi	ng				
Repayment T	erm, Vehicle					

Bond Rate	
Total Annual Cost of Existing Plant	

3

#### Table A-3. Substantial Impacts Analysis – Part I

#### PART I. CALCULATING THE MUNICIPAL AFFORDABILITY SCREENER

This screener is used to evaluate expected impacts to households. It indicates whether community households can afford to pay the total annualized pollution control costs to avoid water quality degradation.

A. Calculate Average Annualized Cost Per Household	degradation.	
1. Calculate the Total Annual Cost of the Project         Interest Rate for Financing $(i) =$		
Interest Rate for Financing (i) =	Household	
Interest Rate for Financing (i) =		
Time Period for Financing (n) =       (years)         Annualization Factor:       (1) $(i + 1)^n - 1$ (1)         Total Capital Cost of Project to be Financed =       (2)         Annual Operating Costs of Project =       (3)         Annualized Capital Cost       (4) $[(1) \times (2)] =$ (5) <b>2. Calculate the Total Annual Cost to Households</b> (5) <b>2. Calculate the Total Annual Cost to Households</b> (6)         Total Annual Cost of Project (5) x Percentage of Total       (6)         Wastewater Flow Attributable to Residential and Municipal       (6)         Total Annual Cost of Existing Plant (\$ ) x       (7)         Percentage of Total Wastewater Flows =       (7)         Total Annual Cost to Households [(6) + (7)] =       (8) <b>3. Calculate the Average Annualized Cost Per Household</b> (9)		
Time Period for Financing $(n) =$ (years)         Annualization Factor:       (i + 1) <sup>n</sup> - 1         Iteration (i + 1) <sup>n</sup> - 1       (1)         Total Capital Cost of Project to be Financed =       (2)         Annual Operating Costs of Project =       (3)         Annualized Capital Cost       (4)         [(1) x (2)] =       (4)         Total Annual Cost of Project [(3) + (4)] =       (5) <b>2. Calculate the Total Annual Cost to Households</b> (5) <b>2. Calculate the Total Annual Cost to Households</b> (6)         Total Annual Cost of Project (5) x Percentage of Total       (6)         Wastewater Flows =       (7)         Total Annual Cost of Existing Plant (\$ ) x       (7)         Percentage of Total Wastewater Flows =       (7)         Total Annual Cost to Households [(6) + (7)] =       (8) <b>3. Calculate the Average Annualized Cost Per Household</b> (9)	Interest Rate for Financing ( $i$ ) =	
Annualization Factor: $i \\ (i + 1)^n - 1$ (1)Total Capital Cost of Project to be Financed =(2)Annual Operating Costs of Project =(3)Annualized Capital Cost(4) $[(1) \times (2)] =$ (5)Total Annual Cost of Project $[(3) + (4)] =$ Total Annual Cost of Project $[(3) + (4)] =$ Total Annual Cost of Project $[(5) \times Percentage of TotalWastewater Flow Attributable to Residential and MunicipalWastewater Flows =(6)Total Annual Cost of Existing Plant ($) \timesPercentage of Total Wastewater Flow S =(7)Total Annual Cost to Households [(6) + (7)] =(8)3. Calculate the Average Annualized Cost Per HouseholdTotal Annual Cost to Households [(8) =(9)$		,
i $(+i) =$ $(1)$ Total Capital Cost of Project to be Financed = $(2)$ Annual Operating Costs of Project = $(3)$ Annualized Capital Cost $(4)$ $[(1) x (2)] =$ $(4)$ Total Annual Cost of Project $[(3) + (4)] =$ $(5)$ <b>2. Calculate the Total Annual Cost to Households</b> Total Annual Cost of Project $(5) x$ Percentage of TotalWastewater Flow Attributable to Residential and MunicipalWastewater Flows = $(6)$ Total Annual Cost of Existing Plant (\$ ) xPercentage of Total Wastewater Flows =Total Annual Cost to Households [ $(6) + (7)$ ] = <b>3. Calculate the Average Annualized Cost Per Household</b> Total Annual Cost to Households (8) =Number of Households (8) =Number of Households (8) =(9)		(years)
Total Capital Cost of Project to be Financed =       (2)         Annual Operating Costs of Project =       (3)         Annualized Capital Cost       (4)         [(1) x (2)] =       (5)         Total Annual Cost of Project [(3) + (4)] =       (5)         2. Calculate the Total Annual Cost to Households       (5)         Total Annual Cost of Project (5) x Percentage of Total       (6)         Wastewater Flow Attributable to Residential and Municipal       (6)         Total Annual Cost of Existing Plant (\$ ) x       (7)         Percentage of Total Wastewater Flows =       (7)         Total Annual Cost to Households [(6) + (7)] =       (8)         3. Calculate the Average Annualized Cost Per Household       (9)		
Total Capital Cost of Project to be Financed =       (2)         Annual Operating Costs of Project =       (3)         Annualized Capital Cost       (4)         [(1) x (2)] =       (5)         Total Annual Cost of Project [(3) + (4)] =       (5)         2. Calculate the Total Annual Cost to Households       (5)         Total Annual Cost of Project (5) x Percentage of Total       (6)         Wastewater Flow Attributable to Residential and Municipal       (6)         Total Annual Cost of Existing Plant (\$ ) x       (7)         Percentage of Total Wastewater Flows =       (7)         Total Annual Cost to Households [(6) + (7)] =       (8)         3. Calculate the Average Annualized Cost Per Household       (9)	$\underline{i}$ (+ i) =	(1)
Total Capital Cost of Project to be Financed =       (2)         Annual Operating Costs of Project =       (3)         Annualized Capital Cost       (4)         [(1) x (2)] =       (5)         Total Annual Cost of Project [(3) + (4)] =       (5)         2. Calculate the Total Annual Cost to Households       (5)         Total Annual Cost of Project (5) x Percentage of Total       (6)         Wastewater Flow Attributable to Residential and Municipal       (6)         Total Annual Cost of Existing Plant (\$ ) x       (7)         Percentage of Total Wastewater Flows =       (7)         Total Annual Cost to Households [(6) + (7)] =       (8)         3. Calculate the Average Annualized Cost Per Household       (9)	$(i + 1)^n - 1$	
Annualized Capital Cost       (4)         [(1) x (2)] =       (5)         Total Annual Cost of Project [(3) + (4)] =       (5)         2. Calculate the Total Annual Cost to Households       (5)         Total Annual Cost of Project (5) x Percentage of Total       (6)         Wastewater Flow Attributable to Residential and Municipal       (6)         Wastewater Flows =       (6)         Total Annual Cost of Existing Plant (\$ ) x       (7)         Percentage of Total Wastewater Flow Attributable to       (7)         Total Annual Cost to Households [(6) + (7)] =       (8)         3. Calculate the Average Annualized Cost Per Household       (9)	Total Capital Cost of Project to be Financed =	
Annualized Capital Cost       (4)         [(1) x (2)] =       (5)         Total Annual Cost of Project [(3) + (4)] =       (5)         2. Calculate the Total Annual Cost to Households       (5)         Total Annual Cost of Project (5) x Percentage of Total       (6)         Wastewater Flow Attributable to Residential and Municipal       (6)         Wastewater Flows =       (6)         Total Annual Cost of Existing Plant (\$ ) x       (7)         Percentage of Total Wastewater Flow Attributable to       (7)         Total Annual Cost to Households [(6) + (7)] =       (8)         3. Calculate the Average Annualized Cost Per Household       (9)		(3)
[(1) x (2)] =       (5)         Total Annual Cost of Project [(3) + (4)] =       (5)         2. Calculate the Total Annual Cost to Households       (5)         Total Annual Cost of Project (5) x Percentage of Total       (6)         Wastewater Flow Attributable to Residential and Municipal       (6)         Wastewater Flows =       (6)         Total Annual Cost of Existing Plant (\$ ) x       (7)         Percentage of Total Wastewater Flow Attributable to       (7)         Total Annual Cost to Households [(6) + (7)] =       (8)         3. Calculate the Average Annualized Cost Per Household       (9)	Annualized Capital Cost	(4)
Total Annual Cost of Project [(3) + (4)] =       (5)         2. Calculate the Total Annual Cost to Households       (5)         Total Annual Cost of Project (5) x Percentage of Total       (6)         Wastewater Flow Attributable to Residential and Municipal       (6)         Wastewater Flows =       (6)         Total Annual Cost of Existing Plant (\$) x       (7)         Percentage of Total Wastewater Flow Attributable to       (7)         Total Annual Cost to Households [(6) + (7)] =       (8)         3. Calculate the Average Annualized Cost Per Household       (9)	$[(1) \times (2)] =$	
2. Calculate the Total Annual Cost to Households         Total Annual Cost of Project (5) x Percentage of Total         Wastewater Flow Attributable to Residential and Municipal         Wastewater Flows =       (6)         Total Annual Cost of Existing Plant (\$) x         Percentage of Total Wastewater Flow Attributable to         Residential and Municipal Wastewater Flows =         (7)         Total Annual Cost to Households [(6) + (7)] =         3. Calculate the Average Annualized Cost Per Household         Total Annual Cost to Households (8) =         Number of Households         (9)		(5)
Total Annual Cost of Project (5) x Percentage of Total         Wastewater Flow Attributable to Residential and Municipal         Wastewater Flows =       (6)         Total Annual Cost of Existing Plant (\$) x         Percentage of Total Wastewater Flow Attributable to         Residential and Municipal Wastewater Flows =         (7)         Total Annual Cost to Households [(6) + (7)] =         (8)         3. Calculate the Average Annualized Cost Per Household         Total Annual Cost to Households (8) =         Number of Households       (9)		
Wastewater Flow Attributable to Residential and Municipal       (6)         Wastewater Flows =       (6)         Total Annual Cost of Existing Plant (\$) x       ) x         Percentage of Total Wastewater Flow Attributable to       (7)         Residential and Municipal Wastewater Flows =       (7)         Total Annual Cost to Households [(6) + (7)] =       (8)         3. Calculate the Average Annualized Cost Per Household       (9)         Mumber of Households       (9)	2. Calculate the Total Annual Cost to Households	
Wastewater Flow Attributable to Residential and Municipal       (6)         Wastewater Flows =       (6)         Total Annual Cost of Existing Plant (\$) x       ) x         Percentage of Total Wastewater Flow Attributable to       (7)         Residential and Municipal Wastewater Flows =       (7)         Total Annual Cost to Households [(6) + (7)] =       (8)         3. Calculate the Average Annualized Cost Per Household       (9)         Mumber of Households       (9)	Total Annual Cost of Project (5) x Percentage of Total	
Total Annual Cost of Existing Plant (\$) x         Percentage of Total Wastewater Flow Attributable to         Residential and Municipal Wastewater Flows =         Total Annual Cost to Households [(6) + (7)] =         3. Calculate the Average Annualized Cost Per Household         Total Annual Cost to Households (8)         Percentage of Households         (9)	Wastewater Flow Attributable to Residential and Municipal	
Percentage of Total Wastewater Flow Attributable to       (7)         Residential and Municipal Wastewater Flows =       (7)         Total Annual Cost to Households [(6) + (7)] =       (8)         3. Calculate the Average Annualized Cost Per Household       (8)         Total Annual Cost to Households (8)       =         Number of Households       (9)	Wastewater Flows =	(6)
Residential and Municipal Wastewater Flows =       (7)         Total Annual Cost to Households [(6) + (7)] =       (8)         3. Calculate the Average Annualized Cost Per Household       (8)         Total Annual Cost to Households (8) =       (9)         Number of Households       (9)	Total Annual Cost of Existing Plant (\$) x	
Total Annual Cost to Households [(6) + (7)] =       (8)         3. Calculate the Average Annualized Cost Per Household       (8)         Total Annual Cost to Households (8)       =         Number of Households       (9)	Percentage of Total Wastewater Flow Attributable to	
3. Calculate the Average Annualized Cost Per Household         Total Annual Cost to Households (8)         Number of Households	Residential and Municipal Wastewater Flows =	(7)
Total Annual Cost to Households (8)       =         Number of Households      (9)	Total Annual Cost to Households [(6) + (7)] =	(8)
Total Annual Cost to Households (8)       =         Number of Households      (9)		
Number of Households(9)		
		(9)
B. Calculate Screener Value:		
	B. Calculate Screener Value:	
<u>Average Annualized Cost Per Household (9)</u> (x 100) =		
Median Household Income% municipal	Median Household Income	
affordability screen (10)		affordability screen (10)

What type of impac Screener Indicate in	t does the Municipa n table below?		
Little Impact	Mid-Range Impact	impact	
< 1.0 %	1.0% - 2.0%		
pollution control cos Mid-Range Impact Large Impact – low	affordability; house		
Is there a need to Affordability Tes range impact)	o proceed to the t? (yes, if large i	-	(yes/no)

3

Table A-4. Substantial Impacts Analysis – Part II

A. EVALUATI	NG THE DEBT	INDICATORS			
Bond Ratin This is a Me		dit Worthiness of a	a Community		
What is Bor	nd Rating of (nar	ne of municipality	)	?	
What is the res	sulting score? (as	ssign score from t	able below)		
Source of Bond Rating					
S&P					
Moody's					
Score	score points				
		Value of Taxable on Residents with	e Property: hin the Community		
(municipality)		Overall Net			(12)

(municipality)						
Over Market Valu	<u>all Net Debt (1</u> ue of Taxable I	(13a)	%			
What is the res	sulting score?					
	Weak	Mid-Range	Strong			
Compare % from 13a	>5%					
Score	1	(14)	_score points			
		(14)				
Explanation o	f Ratings:					
Weak = negative effect on indicator from increased costs for pollution controls						
<u>Mid-Range</u> = u						
<u>Strong</u> = indica	tor can withsta					

3

### Table A-5. Substantial Impacts Analysis – Part II

				ITY TEST (continued	)
	ment Rate: sures the Genera	I Economic Health	of the Community	y	
What is (r	nunicipality)	L	Inemployment Ra	ate?	
		qual to the State's i sign score from tal			
	Weak	Mid-Range	Strong		
Compare unemployme nt rate	Above State Average	State Average	Below State Average		
Score	1	2	3	score	e points

This Measu Capacity	ire Provides an Ov	erall Indication of C	Community Earni	ng	
What is (mi	unicipality)	Media	an Household Inc	ome?	
Is this abov	e, below, or equal	to the State's rate	?		
What is the re	esulting Score? (as	sign score from tal	ble below)	٦	
	Weak	Mid-Range	Strong		
Compare median income	Weak Below State Average	Mid-Range State Average	Strong Above State Average		

3

### Table A-6. Substantial Impacts Analysis – Part II

PLYING IF	IE SECONDARY	AFFORDABILITY T	EST (continued)
NG THE FINA	NCIAL MANAGEME	ENT INDICATORS	
asures Funding	Capacity Available		
(municipality)		_Property Tax Revenue?	(17)
the Full Marke	t Value of Taxable F	Property?	(18)
Market Value o	of Taxable Property		% (18a)
Weak	Mid-Range	Strong	
<2%	2% - 4%	>4%	
	<b>/ Tax Revenue</b> asures Funding nunity's Wealth (municipality) _ the Full Marke roperty Tax Re Market Value o		(municipality) Property Tax Revenue? the Full Market Value of Taxable Property? roperty Tax Revenue (17) (x 100) = Market Value of Taxable Property (18) sulting Score? (assign score from table below)

	perty Tax Col	lection Rate of (mun	icipality)	%_
Vhat is the resu	ulting Score?	(assign score from ta	able below)	
	Weak	Mid-Range	Strong	
Compare tax collection rate	<94%	94% - 98%	>98%	
		2		 score points (20
CALCULATI	E THE CUMU This is the av	LATIVE SECONDA	RY AFFORDAB	
0. CALCULAT EST SCORE: bove. (11) + (14) +	E THE CUMU This is the av (15) + (16) + 6	LATIVE SECONDA	RY AFFORDAB	 score points (20)
0. CALCULAT EST SCORE: bove. (11) + (14) +	E THE CUMU This is the av (15) + (16) + 6	VERATIVE SECONDA verage score of all th (19) + (20) =	RY AFFORDAB	

2

		al Impacts Analy	sis – Part III	
Part III. Assessm	ent of Substanti	al Impacts Matrix		
THE MUNICIPAL .	AFFORDABILITY	SCREENER (10) =		%
THE CUMULATIV	E SECONDARY		EST SCORE (21) =	score points
Where does (muni Substantial Impact			appear in the	
1	Substanti	al Impacts Matrix		
Secondary Assessment Score	Munio	cipal Affordability Scre	eener	
	<1.0%	1.0% - 2.0%	>2.0%	
< 1.5	?	X	Х	
1.5 – 2.5	$\checkmark$	?	Х	
> 2.5	$\checkmark$	$\checkmark$	?	
? = Questionab √ = Community X = Community	can afford the p	oollution control he pollution control		
afford, not afford,	or questionable)	of the (municipality)		Matrix Result
n other words, cai o avoid water qua			ide the facility in order	
	nable Affordabili	al Impacts analysis is y", then proceed to th ion.		Complete Widespread Impacts Analysis? (yes/no)

2

#### Table A-8. Widespread Impacts Analysis – Public Facility

#### 1. Define the Affected Community

Evaluate the Discharger's Contribution to the Community:

- Contribution to economic base (e.g., property taxes and employment)
- Provides product or service upon which other businesses or the community depend

#### 2. Evaluate Community's Current Characteristics

Evaluate how community's current socioeconomic health may change if proposed project must avoid degradation to water quality by considering the following factors:

- Median household income
- o Unemployment rate
- Rate of industrial development
- Developing and declining industries
- Percent of households below poverty line
- Ability of community to carry more debt
- Local and regional factors

Other applicable information on the local and regional economy that should also be reviewed includes:

- Annual rate of population change
- Current financial surplus as a percentage of total expenditures
- Percentage of property taxes actually collected
- Property tax revenues as a percentage of the market value of real property
- Overall debt outstanding as a percentage of market value of real property
- Overall debt per capita
- Percentage of outstanding debt due within 5 years

#### 3. Evaluate How Community Characteristics Would Change if Discharger Must Avoid Degradation to Water Quality

Evaluate the projected adverse socioeconomic impacts of adding pollution controls to the project to meet antidegradation requirements by considering the following:

- Property Values
- o Employment Rate
- o Commercial Development Opportunities
- o Tax Revenues
- Expenditure on Social Services
- State level impacts such as loss of revenues and increased expenditures

#### 1 **APPENDIX – B Tier 2 Review of a Private Facility**

Appendix B includes additional information that may be required by the Department to evaluate socio-economic factors of a private facility during a Tier 2 review. This evaluation is based on two types of impacts, referred to as "substantial" and "widespread". The Substantial Impacts analysis is found in Table 2. The Widespread Impacts analysis is found in Table 3.

#### 8 SUBSTANTIAL IMPACTS - SUMMARY

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10 <u>Purpose of Substantial Impacts analysis:</u> Determine whether a private facility can afford 11 pollution controls in order to avoid any degradation of water quality.

12

The first step in a Substantial Impacts analysis is to provide data on the socio-economic factors listed in the worksheet in Table 1. This data is then used to calculate four financial tests that in turn indicate the financial health of a private entity (Table 2).

16

#### 17 WIDESPREAD IMPACTS - SUMMARY

18

Purpose of widespread impacts analysis: Evaluates the social costs of pollution control
 requirements by: 1) Defining the affected community; 2) Evaluating the community's
 current characteristics; and 3) Evaluating how community characteristics would change
 if discharger must avoid degradation to water quality.

23

If the Substantial Impacts analysis (i.e., the four financial tests) indicates that the private entity's financial health is questionable, then a Widespread Impacts analysis may be completed to further resolve the affordability issue. This analysis is primarily a qualitative evaluation based on community socioeconomic factors that are expanded to a larger scale than the Substantial Impacts analysis.

#### 2 3

#### Table B-1. Data Worksheet for Financial Factors

Financial Factor	Data
Current Assets	
Current Liabilities	
Cash flow per given year	
Total debt of the entity	
Amount firm has borrowed (debt)	
Amount of stockholders' capital (equity)	
Pre-tax earnings	
Annualized pollution control cost	

# Table B-2. Substantial Impacts Analysis - Financial Tests Used to Measure the Financial Health of a Private Entity

4

**1. Liquidity Test** - Indicates how easily an entity can pay its short-term bills.

Current Ratio = Current Assets / Current Liabilities

NOTE: A ratio greater that 2 indicates affordability

2. Solvency Test - Indicates how easily an entity can pay its fixed and long-term bills.

Beaver's Ratio = Cash flow per given year / Total debt of the entity

NOTE: > 0.20 Indicates private entity is solvent < 0.15 Indicates private entity may go bankrupt

3. Leverage Test - Indicates how much money the entity can borrow.

Debt-to-Equity Ratio = Amount firm has borrowed (debt) / Amount of Stockholders' capital (equity)

NOTE: The larger the Debt-to-Equity Ratio, the less likely that the entity will be able to borrow funds

**4. Earnings Test** - Indicates how much the entity's profitability will change with the additional pollution control needed to avoid degradation of water quality.

Earnings = Pre-tax – Annualized Pollution Control Cost

NOTE: Compare earnings result with entity's revenues to measure post-compliance profit rate

#### Guidelines to evaluate financial tests:

- Results of all four tests above should be considered jointly
- Ratios and tests should be compared over several years
- Financial ratios should also be compared against those of "healthy" entities
- o The role the entity plays in a parent firm's operations should also be considered

1		
2 3		Table B-3. Widespread Impacts Analysis – Private entity/facility
4 5	1.	Define the Affected Community
6 7 8 9		<ul> <li>Evaluate the Discharger's Contribution to the Community:</li> <li>Contribution to economic base (e.g., property taxes and employment)</li> <li>Provides product or service upon which other businesses or the community depend</li> </ul>
10 11	<u>2.</u>	Evaluate Community's Current Characteristics
12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30		<ul> <li>Evaluate how community's current socioeconomic health would change if proposed project must avoid degradation to water quality by considering the following factors: <ul> <li>Median household income</li> <li>Unemployment rate</li> <li>Rate of industrial development</li> <li>Developing and declining industries</li> <li>Percent of households below poverty line</li> <li>Ability of community to carry more debt</li> <li>Local and regional factors</li> </ul> </li> <li>Other applicable information on the local and regional economy that should also be reviewed includes: <ul> <li>Annual rate of population change</li> <li>Current financial surplus as a percentage of total expenditures</li> <li>Percentage of property taxes actually collected</li> <li>Property tax revenues as a percentage of the market value of real property</li> <li>Overall debt outstanding as a percentage of market value of real property</li> <li>Overall debt per capita</li> </ul></li></ul>
31		<ul> <li>Percentage of outstanding debt due within 5 years</li> </ul>
32 33 34	<u>3.</u>	Evaluate How Community Characteristics Would Change if Discharger Must Avoid Degradation to Water Quality
35 36 37 38 39 40 41		Evaluate the projected adverse socioeconomic impacts of adding the pollution control to the project to meet antidegradation requirements by considering the following:
42 43 44		<ul> <li>Tax Revenues</li> <li>Expenditure on Social Services</li> <li>State level impacts such as loss of revenues and increased expenditures</li> </ul>

### **APPENDIX – C Assimilative Capacity Calculation Guideline**

The intent of this guideline is to provide a screening tool that will allow an estimate of
the magnitude of the impact of a discharge on receiving water (i.e., *de minimis* or not).

6 This guideline and accompanying spreadsheets are intended to serve as a guideline for 7 calculation of assimilative capacity for purposes of the Antidegradation Implementation Procedure. This procedure is intended only for use in these guidelines. Where the 8 9 Procedure calls for calculation of assimilative capacity, the value is used as a screening tool to determine if a proposed discharge will have *de minimis* effects or not. Since this 10 is a screening tool, that is not being used for more rigorous determinations such as 11 12 calculating enforceable NPDES permit effluent limits or TMDL waste load allocations, 13 the method has been kept as simple as possible and is viewed as an estimate. Users of this guideline may find it necessary in the course of events to slightly modify the 14 process in order to accommodate unique problems with data sets or circumstances that 15 might occur. 16

17

18 The spreadsheets illustrate the calculations to estimate assimilative capacity. The first 19 set of calculations addresses pollutants other than Biochemical Oxygen Demand 20 (BOD). The second set of calculations addresses BOD. The second set of calculations 21 is necessary because BOD is the parameter regulated in discharge permits to prevent 22 undue depletion of Dissolved Oxygen (DO) in receiving waters.

23

The following data gathering guidelines should be used to compile the information required for the two sets of calculations. However, because of variations in data availability, as well as other relevant case-specific factors, the guidelines may be adjusted to ensure the compilation of appropriate information. In circumstances indicating the need to adjust the guidelines, the reviewer should consult with the Department, as well as other NMED water quality assessment protocols and Quality Assurance Plans.

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- 32 Data Gathering Guidelines.
- 1) Obtain ambient water quality data for the pollutant of concern in the receiving water
   upstream but as close to the discharge as possible. Optimally, use the water quality
   station and data used by NMED SWQB in the most recent evaluation of the stream
   segment for purposes of the biennial Clean Water Act Section 303(d) evaluation.
- a) Possible sources of data include:
  - i) NMED SWQB water quality database
  - ii) USEPA STORET
    - iii) USGS water quality monitoring stations
  - b) Use all valid data points regardless of the stream flow or time of year when collected
- 43 c) Valid data is data that has met quality assurance / quality control protocols
   44 established by the SWQB
- 45 2) Obtain data about the discharge.

1	a) Describle as seen of data is data
1	a) Possible sources of data include:
2	i) NPDES Permit Applications
3	(1) Supplemental sampling requested by the permitting authority to support
4	the permitting process may be used.
5	ii) USEPA STORET
6	iii) USEPA Permit Compliance System (PCS)
7	iv) Other valid data that has met quality assurance / quality control protocols
8	established by the SWQB
9	3) Summarize the data by calculating the arithmetic mean for all parameters except
10	bacteria. Use geometric mean to summarize bacteria data. This value will be used
11	as the upstream concentration in the calculation below.
12	a) If the data value is reported as less than a number, that usually means the test
13	result was below the lab's minimum quantification level.
14	<ol> <li>If all data points are "less than"; treat them all as zeros.</li> </ol>
15	ii) If some of the data are "less than" and some are quantified values, use the
16	actual quantified values and one half of the "less than" value to calculate the
17	geometric mean.
18	(1) For example in a data set that has the following 4 values: 1.2, <0.5, <0.6
19	and 1.4, input the following numbers into the calculation 1.2, 0.25, 0.3 and
20	1.4. The result in this example would be 0.6
21	<ol><li>Obtain critical low flow data for the stream above the discharge.</li></ol>
22	a) Critical low flow for purpose of the calculation is the minimum average four
23	consecutive day flow which occurs with a frequency of once in three years (4Q3)
24	i) In most cases it will only be necessary to find the 4Q3. However if the only
25	concern is estimating the assimilative capacity necessary to meet a human
26	health criterion then the harmonic mean flow may be substituted.
	-

Calculation of Assimilative Capacity Parameters	other th	an BOD			
Step 1 - Collect Basic Information	1		1		1
(Instructions: Fill in yellow boxes - Spreadsheet will calculate blue boxes)					
Upstream Data	Symbol	Value	Units		
critical low flow of stream (4Q3)	Qu	22	cfs		
pollutant concentration	Cu	0.01	mg/L		
•			Ŭ		
Effluent Data					
design flow (existing) [if new discharge use 0]	Qe	1.50	cfs		
design flow (proposed)	Qp	2.30	cfs		
existing pollutant limit concentration [if new discharge use 0]	Ce	0.10	mg/L		
proposed pollutant limit concentration [use Ce if no change is proposed]	Cx	0.10	mg/L		
Downstream Data					
water quality criterion for pollutant of concern	Cs	0.50	mg/L		
downstream flow under 4Q3 conditions with existing discharge (Qu + Qe)	Qd	23.50	cfs		
downstream flow under 4Q3 conditions with proposed discharge ( $Qu + Qe$ )	Qx	24.30	cfs		
	QA	24.00	010		
Constants					
conversion factor for (mg/L to lbs/day)	cf	8.34			
Ston 2 Determine Available Bollutant Assimilative Conseity with the					
Step 2 - Determine Available Pollutant Assimilative Capacity with the Discharge at Existing & Proposed Design Flows	Ourseland	Malua	Linite		
	Symbol	Value	Units		1
waterbody pollutant assimilative capacity (Qx*Cs*cf)	Ac Lb	101.33	lbs/day		
background pollutant load (Qu*Cs*cf)		1.83	lbs/day		
existing permit load (Qe*Ce*cf)	Le	1.25	lbs/day		
proposed permit load (Qp*Cu*cf)	Ln	1.92	lbs/day		
Remaining Assimilative Capacity with existing discharge (Ac-Lb-Le)	Ae	98.25	lbs/day		
Remaining Assimilative Capacity with proposed discharge (Ac-Lb-Ln)	An	97.58	lbs/day		
					1
Step 3 - Determine if proposed new or added discharge is <i>de minimis</i>					
or if a full antidegradation review will be required. Antideg review is					
required if the new discharge will consume greater than 10% of the					
remaining assimilative capacity. Discharges that consume 10% or less					
of the remaining assimilative capacity will be considered "de minimis"					
and do not require a full antidegradation review.	<u>Symbol</u>	Value	<u>Units</u>		
10% of Remaining Assimilative Capacity [prior to new discharge] (Ae*0.1)	Ar	9.82	lbs/day		
Added Capacity Utilization by new discharge (Ae-An)	Au	0.67	lbs/day		
	,	0.07			+
Determine if Antideg review is required or if new discharge is "de minimis"					
If $Ar > Au$ then the discharge is de minimis. If $Ar < or = Au$ then an			inimis		+
antidegradation review is required.		disch	narge		
Helpful Tools					
Convert million gallons per day [mgd] to cubic feet per second [cfs] (mgd / 0.646272)		1.50	mgd	2.32	cfs
Convert micrograms [ug] to milligrams [mg] (ug / 1000)		1.00	ug	0.001	mg

1	Α	В	С	D
1	Calculation of Assimilative Capacity BOD/DO			
2	Based upon Streeter-Phelps Model in Hammer, M.J., 1975. Water and Waste-Water Technology	ogy. Wiley &	Sons, Inc.	
3	Step 1 - Collect Basic Information			
4	(Instructions: Fill in yellow boxes - Spreadsheet will calculate blue	e boxes)		
5				
6	Upstream Data	<u>Symbol</u>	Value	<u>Units</u>
7	critical low flow of stream (4Q3)	Q1	22	cfs
8	Biochemical Oxygen Demand - 5-day (BOD5)	B1	2	mg/L
9	Dissolved Oxygen (DO)	D1	8.2	mg/L
	Temperature	T1	17	Deg.C.
11	Conductivity	C1	500	uS/cm
12				
13	Effluent Data			
	design flow (existing)	Q2	1.5	cfs
	design flow (proposed)	Q3	1.8	cfs
	Biochemical Oxygen Demand - 5-day (BOD5) [use current permit limit or secondary			
16	treatment limit - usually 30 mg/I]	B2	30	mg/L
	Biochemical Oxygen Demand - 5-day (BOD5) [use proposed permit limit or secondary			Ŭ
17	treatment limit - usually 30 mg/l]	B3	30	mg/L
	Dissolved Oxygen (DO) (existing)	D2	3	mg/L
	Dissolved Oxygen (DO) (proposed)	D3	3	mg/L
	Temperature (existing)	T2	18	Deg.C.
	Temperature (proposed)	T3	18	Deg.C.
	altitude of facility (feet above sea level)	а	5000	feet
	conductivity (existing)	C2	500	uS/cm
	conductivity (proposed)	C3	500	uS/cm
25				
26	Downstream Data			
	enter water quality criterion for D.O. below discharge	WQ	5.0	mg/L
28	enter mean velocity of flow, feet per second (below discharge)	V	0.6	ft./sec
	enter mean depth of flow, feet (below discharge)	h	4	feet
	depays genetics rate per day @ 20 deg C (A depays genetics rate may be determined in			
	deoxygenation rate, per day @ 20 deg C (A deoxygenation rate may be determined in the laboratory, typical rates vary between 0.05 and 0.2. If unknown use 0.1. The actual			
	rate is not greatly important to this exercise because the intent is to <u>estimate</u> the relative			
30	impact of a new discharge not a precise impact.)	k1	0.1	
31				
	Step 2 - Calculate Downstream Concentrations Based Upon Mixing			
33	Downstream Data			
	calculate existing BOD concentration based upon mixing (existing scenario)			
34	[cbe=((Q1*B1)+(Q2*B2))/(Q1+Q2)]	Cbe	3.8	mg/L
	calculate existing DO concentration based upon mixing (existing scenario)			
35	[Cde=((Q1*D1)+(Q2*D2))/(Q1+Q2)]	Cde	7.9	mg/L
1	calculate existing Temperature based upon mixing (existing scenario)			
1			474	Deg.C.
36	[Cte=((Q1*T1)+(Q2*T2))/(Q1+Q2)]	Cte	17.1	Deg.e.
36		Cte	17.1	Dog.o.
37	[Cte=((Q1*T1)+(Q2*T2))/(Q1+Q2)]	Cte Cce	500.0	uS/cm
	[Cte=((Q1*T1)+(Q2*T2))/(Q1+Q2)] calculate <b>existing</b> Conductivity based upon mixing (existing scenario) [Cce=((Q1*C1)+(Q2*C2))/(Q1+Q2)]			
37 38	[Cte=((Q1*T1)+(Q2*T2))/(Q1+Q2)] calculate <b>existing</b> Conductivity based upon mixing (existing scenario) [Cce=((Q1*C1)+(Q2*C2))/(Q1+Q2)] calculate <b>projected</b> BOD concentration based upon mixing (proposed scenario)			
37 38	[Cte=((Q1*T1)+(Q2*T2))/(Q1+Q2)] calculate <b>existing</b> Conductivity based upon mixing (existing scenario) [Cce=((Q1*C1)+(Q2*C2))/(Q1+Q2)] calculate <b>projected</b> BOD concentration based upon mixing (proposed scenario) [Cbp=((Q1*B1)+(Q3*B3))/(Q1+Q3)]			
37 38	[Cte=((Q1*T1)+(Q2*T2))/(Q1+Q2)] calculate <b>existing</b> Conductivity based upon mixing (existing scenario) [Cce=((Q1*C1)+(Q2*C2))/(Q1+Q2)] calculate <b>projected</b> BOD concentration based upon mixing (proposed scenario)	Cce	500.0	uS/cm
37 38 39	[Cte=((Q1*T1)+(Q2*T2))/(Q1+Q2)] calculate <b>existing</b> Conductivity based upon mixing (existing scenario) [Cce=((Q1*C1)+(Q2*C2))/(Q1+Q2)] calculate <b>projected</b> BOD concentration based upon mixing (proposed scenario) [Cbp=((Q1*B1)+(Q3*B3))/(Q1+Q3)] calculate <b>projected</b> DO concentration based upon mixing (proposed scenario) [Cdp=((Q1*D1)+(Q3*D3))/(Q1+Q3)]	Cce	500.0	uS/cm
37 38 39	[Cte=((Q1*T1)+(Q2*T2))/(Q1+Q2)] calculate <b>existing</b> Conductivity based upon mixing (existing scenario) [Cce=((Q1*C1)+(Q2*C2))/(Q1+Q2)] calculate <b>projected</b> BOD concentration based upon mixing (proposed scenario) [Cbp=((Q1*B1)+(Q3*B3))/(Q1+Q3)] calculate <b>projected</b> DO concentration based upon mixing (proposed scenario)	Cce Cbp	500.0 4.1	uS/cm mg/L

calculate projected Conductivity based upon mixing (existing scenario)         Ccp         500.0         us/km           43         Iccp=((C1*C1)+(C3*C3))/(C1+C3)]         Ccp         500.0         us/km           44         Step 3 - Streeter-Phelps Estimate O Oxygen Sag - Deoxygenation and Reseration Coefficients		A	В	С	D
A         Step 3 - Streeter-Phelps Estimate of Oxygen Sag - Deoxygenation and Reaeration Coefficients           45         Estimate Deoxygenation Coefficients         Image: Comparison of Coefficients           46         Image: Coefficients         Image: Coefficients           47         Calculate temperature adjusted k1 rate for proposed scenario [k1=k1*1.047*(Cte-20)]         K1p         0.09           48         Calculate temperature adjusted k1 rate for proposed scenario [k1=k1*1.047*(Cte-20)]         k2         0.31           52         Calculate temperature adjusted k2 rate for existing scenario [k2=k2*1.015*(Cte-20)]         k2         0.30           53         Calculate temperature adjusted k2 rate for existing scenario [k2=k2*1.015*(Cte-20)]         k2p         0.30           54         Calculate temperature adjusted k2 rate for proposed scenario [k2=k2*1.015*(Cte-20)]         k2p         0.30           55         Step 4 - Streeter-Phelps - Estimate Dissolved Oxygen Demand, proposed scenario [L0=Cbp/(1-10*]         Lop         6.0           56         Strip (1)         Estimate Ultimate Biochemical Oxygen Deficits         Estimate Ultimate Biochemical Oxygen Deficits         10           58         Calculate Dissolved Oxygen Saturation for the facility's altitude at temp ctp [d1= (14.62-1)         10         8.0         mg/L           61         Calculate Oxygen Deficit for proposed scenario [De=ldp-cdp]			Сср	500.0	uS/cm
Bit         Estimate Deoxygenation Coefficients           46         47         calculate temperature adjusted k1 rate for existing scenario [k1e+k1*1.047^(Cte-20)]         K1e         0.09           48         calculate temperature adjusted k1 rate for proposed scenario [K1p+k1*1.047^(Cte-20)]         K1p         0.09           49         Calculate temperature adjusted k1 rate for existing scenario [R2e+R2*1.015^(Cte-20)]         k2         0.30           51         Estimate Reaeration Coefficients and Ultimate BDD         k2         0.30           52         calculate temperature adjusted k2 rate for existing scenario [R2e+R2*1.015^(Cte-20)]         k2p         0.30           53         calculate temperature adjusted k2 rate for proposed scenario [R2e-R2*1.015^(Cte-20)]         k2p         0.30           54         Step 4 - Streeter-Phelps - Estimate Dissolved Oxygen Deficits, Time & Distance to Minimum DO         55           55         Estimate Ultimate Biochemical Oxygen Deficits         6.0         6.0           73         Strill)         Eatimate Dissolved Oxygen Saturation for the facility's altitude at temp ctp [Idp = (14.62-Idp 8.0         mg/L           60         0.3898*Cle)+(0.006696*Cler/2)-(0.00005897*(Cler/3)))*(1-0.00000697*a)^s.1617         Idp 8.0         mg/L           61         calculate Initial Dissolved Oxygen Deficit for existing scenario [De=Idp-cdp]         De         0.2		Step 3 - Streeter-Phelps Estimate of Oxygen Sag - Deoxygenation and Reaeration Co	efficients	S	
46       1         47       calculate temperature adjusted k1 rate for existing scenario [k1p=k1*1.047^(Cte-20)]       K1p       0.09         48       calculate temperature adjusted k1 rate for proposed scenario [k1p=k1*1.047^(Cte-20)]       K1p       0.09         50       Estimate Reseration Coefficients and Ultimate BOD       k2       0.31         51       calculate remerature adjusted k2 rate for existing scenario [k2e=k2*1.015^(Cte-20)]       k2e       0.30         53       calculate temperature adjusted k2 rate for existing scenario [k2e=k2*1.015^(Ctp-20)]       k2e       0.30         54       calculate temperature adjusted k2 rate for proposed scenario [k2e=k2*1.015^(Ctp-20)]       k2e       0.30         54       calculate timitate Biochemical Oxygen Demand, existing scenario [L0e=Cbe/(1-10^(-       Loe       6.5         55       Step 4 - Streeter-Phelps - Estimate Dissolved Oxygen Deficits, Time & Distance to Minimum DO       Estimate Ultimate Biochemical Oxygen Deficits       Lop       6.0         58       Calculate Initial Dissolved Oxygen Deficits       Lop       6.0       6.0       6.0         59       Calculate Initial Dissolved Oxygen Deficit for existing scenario [Del-(de-(de)       De       0.1       mg/L         61       calculate Initial Dissolved Oxygen Deficit for existing scenario [Del-(de-(de)       De       0.1       mg/L </td <td></td> <td></td> <td></td> <td></td> <td></td>					
activate temperature adjusted k1 rate for proposed scenario [K1p=k1*1.047×(Ctp-20)]         K1p         0.09           30         Estimate Reaeration Coefficients and Ultimate BOD         k2         0.31           51         calculate reaeration rate, per day @ 20 deg C [k2=33'(v(h^1.33)]         k2         0.30           52         calculate remerature adjusted k2 rate for existing scenario [k2p=k2*1.015×(Ctp-20)]         k2p         0.30           53         calculate temperature adjusted k2 rate for proposed scenario [k2p=k2*1.015×(Ctp-20)]         k2p         0.30           54         Step 4 - Streeter-Phelps - Estimate Dissolved Oxygen Deficits, Time & Distance to Minimum DO         Estimate Ultimate Biochemical Oxygen Demand, existing scenario [Lop=Cbp/(1-10×[-         Loe         6.5           55         Galculate Initial Dissolved Oxygen Deficits         calculate Initial Dissolved Oxygen Deficits         calculate Initial Dissolved Oxygen Deficits           60         0.3989*Cte)+(0.0066989*Ctex2))-(0.00006897*(tex^3)))*(1-0.0000697*a)x5.167         Ide         8.0         mg/L           61         calculate Dissolved Oxygen Deficit for existing scenario [b=(de-cde]         De         0.1         mg/L           62         calculate Initial Dissolved Oxygen Deficit for proposed scenario [b=(de/cdp]         De         0.1         mg/L           63         calculate Initial Dissolved Oxygen Deficit for existing scenario [te=(1/	46				
410         K1p         0.009           50         Estimate Reaeration Coefficients and Utimate BOD         1           51         calculate reaeration rate, per day @ 20 deg C [k2=3.3*(v(h*1.33)]         k2         0.30           52         calculate temperature adjusted k2 rate for existing scenario [k2e=k2*1.015^(Ctp-20)]         k2e         0.30           53         calculate temperature adjusted k2 rate for proposed scenario [k2p=k2*1.015^(Ctp-20)]         k2p         0.30           54         Step 4 - Streeter-Phelps - Estimate Dissolved Oxygen Deficits, Time & Distance to Minimum DO         Estimate Ultimate Biochemical Oxygen Demand, existing scenario [L0=Cbe/(1-10^{-1})         L0e         5.5           55         Calculate Initial Dissolved Oxygen Deficits         1         0         6.0           58         Calculate Initial Dissolved Oxygen Deficits         1         0         6.0           58         Calculate Dissolved Oxygen Saturation for the facility's altitude at temp ctp [lde=(14.62-(0.3898*Cte)+(0.006969*(ctp-2))+(0.00005897*(cte^-3)))*(1-0.0000697*9)*5.167         ldp         8.0         mg/L           50         calculate Initial Dissolved Oxygen Deficit for existing scenario [De=ldp-cde]         De         0,1         mg/L           61         (0.3898*Cte)+(0.006969*(ctp-2))+(0.00005897*(ctp-3)))*(1-0.0000697*9)*5.167         ldp         8.0         mg/L	47	calculate temperature adjusted k1 rate for existing scenario [k1e=k1*1.047^(Cte-20)]	K1e	0.09	
EV         Estimate Reservation Coefficients and Ultimate BOD         view         view           51         calculate reaeration rate, per day @ 20 deg C [k2=3.3'(vi(h^1.3)]         k2         0.30           52         calculate temperature adjusted k2 rate for existing scenario [k2p=k2*1.015^(Ctp-20)]         k2p         0.30           53         calculate temperature adjusted k2 rate for proposed scenario [k2p=k2*1.015^(Ctp-20)]         k2p         0.30           54         Step 4 - Streeter-Phelps - Estimate Dissolved Oxygen Deficits, Time & Distance to Minimum DO         Estimate Ultimate Biochemical Oxygen Demand, existing scenario [Lop=Cbp/(1-10^{-1.55} 5'kT)])         Lop         6.0           55         Strip)         Estimate Ultimate Biochemical Oxygen Deficits         6.0         6.0           59         Calculate Initial Dissolved Oxygen Deficits         6.0         6.0         6.0           61         Calculate Initial Dissolved Oxygen Saturation for the facility's altitude at temp ctp [ldp = (14.62- ldp 8.0 mg/L calculate Initial Dissolved Oxygen Deficit for existing scenario [De=ide-cde]         De         0.1 mg/L calculate Initial Dissolved Oxygen Deficit for existing scenario [De=ide-cde]         De         0.1 mg/L calculate Initial Dissolved Oxygen Deficit for existing scenario [De=ide-cde]         De         0.1 mg/L calculate Initial Dissolved Oxygen Deficit for existing scenario [De=ide-cde]         De         0.1 mg/L calculate Initial Dissolved Oxygen Deficit for existing scenario [De=ide-cde]		calculate temperature adjusted k1 rate for proposed scenario [K1p=k1*1.047^(Ctp-20)]	K1p	0.09	
52       calculate temperature adjusted k2 rate for existing scenario [k2=k2*1.015^(Cte-20)]       k2e       0.30         53       calculate temperature adjusted k2 rate for proposed scenario [k2=k2*1.015^(Ctp-20)]       k2p       0.30         54       0       0       0         55       Step 4 - Streeter-Phelps - Estimate Dissolved Oxygen Deficits, Time & Distance to Minimum DO         56       S*r(1)]       Loe       5.5         Estimate Ultimate Biochemical Oxygen Demand, proposed scenario [L0=Cbp/(1-10^-)       Loe       6.0         58       -       -       -       -         59       Calculate Initial Dissolved Oxygen Deficits       -       -       -         calculate Dissolved Oxygen Saturation for the facility's altitude at temp ctp [Ide = (14.62-       -       -       -         60       (0.3898*Cte)+(0.006969*Cte^>2)-(0.0000589*7(Cte^3)))*(1-0.0000697*a)^5.167       Ide       8.0       mg/L         calculate Dissolved Oxygen Deficit for existing scenario [De=ldp-cdp]       Dp       0.2       mg/L         61       Calculate Initial Dissolved Oxygen Deficit for proposed scenario [De=ldp-cdp]       Dp       0.2       mg/L         62       calculate Initial Dissolved Oxygen Deficit for proposed scenario [De=(1/(k2e-       -       -       -         64       -       -<		Estimate Reaeration Coefficients and Ultimate BOD			
53         calculate temperature adjusted k2 rate for proposed scenario [k2p=k2*1.015^(Ctp-20)]         k2p         0.30           54         Step 4 - Streeter-Phelps - Estimate Dissolved Oxygen Deficits, Time & Distance to Minimum DO         55           55         Step 4 - Streeter-Phelps - Estimate Dissolved Oxygen Deficits, Time & Distance to Minimum DO         5.5           56         5*(1))]         Loe         5.5           57         S'(1))]         Loe         6.0           58         Calculate Initial Dissolved Oxygen Deficits         6.0           59         Calculate Initial Dissolved Oxygen Saturation for the facility's altitude at temp ctp [Idp = (14.62-(0.3898*Ctp)+(0.006969*Ctp^2))-(0.00006897*(Ctp^3)))*(1-0.0000697*a)^5.167         Idp         8.0         mg/L           61         calculate Dissolved Oxygen Saturation for the facility's altitude at temp ctp [Idp = (14.62-(0.3898*Ctp)+(0.006969*(ctp^2))-(0.00005897*(ctp^3)))*(1-0.0000697*a)^5.167         Idp         8.0         mg/L           62         calculate Initial Dissolved Oxygen Deficit for rexisting scenario [De=Idp-cdp]         Dp         0.2         mg/L           63         calculate time of Travel to Minimum DO of sag curve for existing scenario [tp=(1/(k2e-tp)/(tp)/(tp)/(k2e-k1e)/(tp)/(k2e-k1e)/(tp)/(k2e-k1e)/(k1e^+L0e)))))))         0.1         mg/L           64         calculate time of travel to minimum DO of sag curve for proposed scenario [tp=(1/(k2e-tp)/(tp)/(tp)/(tp)/(tp)/	51	calculate reaeration rate, per day @ 20 deg C [k2=3.3*(v/(h^1.33)]	k2	0.31	
33         R2p         U.30           54         54         54           55         Step 4 - Streeter-Phelps - Estimate Dissolved Oxygen Deficits, Time & Distance to Minimum DO           56         Step 4 - Streeter-Phelps - Estimate Dissolved Oxygen Demand, existing scenario [L0e=Cbe/(1-10^{-1})/(-10^{-1}	52	calculate temperature adjusted k2 rate for existing scenario [k2e=k2*1.015^(Cte-20)]	k2e	0.30	
Step 4 - Streeter-Phelps - Estimate Dissolved Oxygen Deficits, Time & Distance to Minimum DO           55         Estimate Ultimate Biochemical Oxygen Demand, existing scenario [Loe=Cbe/(1-10^(- 5'K1))]         Loe         5.5           57         Step 4 - Streeter-Phelps - Estimate Oxygen Demand, proposed scenario [Lop=Cbp/(1-10^(- 5'K1))]         Lop         6.0           58         Calculate Initial Dissolved Oxygen Deficits		calculate temperature adjusted k2 rate for proposed scenario [k2p=k2*1.015^(Ctp-20)]	k2p	0.30	
Loc         Estimate Ultimate Biochemical Oxygen Demand, existing scenario [Loe=Cbe/(1-10^(- 5'K1))]         Loe         5.5           5'K1))         Estimate Ultimate Biochemical Oxygen Demand, proposed scenario [Lop=Cbp/(1-10^(- 5'K1))]         Lop         6.0           5'S         Calculate Initial Dissolved Oxygen Deficits	54				
56         5*(1))         Loe         5.5           Estimate Ultimate Biochemical Oxygen Demand, proposed scenario [Lop=Cbp/(1-10^{-5})]         Lop         6.0           57         5*(1))         Lop         6.0           58         Calculate Initial Dissolved Oxygen Deficits         Lop         6.0           60         Calculate Initial Dissolved Oxygen Saturation for the facility's altitude at temp ctp [Idp = (14.62-(0.3898*Ctp)+(0.006969*Cte*2))-(0.00005897*(ctp*3)))*(1-0.0000697*a)*5.167         Idp         8.0         mg/L           61         Calculate Initial Dissolved Oxygen Deficit for existing scenario [De=Ide-cde]         De         0.1         mg/L           62         calculate Time of Travel to Minimum DO Sag         Calculate time of travel to minimum DO of sag curve for existing scenario [De=Idp-cdp]         Dp         0.2         mg/L           64         Calculate time of travel to minimum DO sag curve for proposed scenario [tp=(1/(k2p- K1p))*(log(((k2p/k1p)*(1-(Dp*(k2p-K1p)/(k1p*L0p)))))))         tp         2.4         days           68         Calculate Distance Downstream to Minimum DO Sag existing scenario [Me=(te*v*86400) seconds per day)/5280 feet per mile)]         Mp         23.5         miles           73         Step 4 - Streeter-Phelps - Estimate Dissolved Oxygen Deficits at Critical Time         1.0         mg/L           73         Step 4 - Streeter-Phelps - Estimate Dissolved Oxygen	55	Step 4 - Streeter-Phelps - Estimate Dissolved Oxygen Deficits, Time & Distance to Mi	nimum D	0	
67         5*k1))]         Lop         6.0           58         Calculate Initial Dissolved Oxygen Deficits	56	5*k1))]	L0e	5.5	
59         Calculate Initial Dissolved Oxygen Deficits         mg/L           calculate Dissolved Oxygen Saturation for the facility's altitude at temp cte [Ide=(14.62- (0.3898°Cte)+(0.006969°Cte^2))-(0.00005897*(Cte^3)))*(1-0.0000697*a)^5.167]         Ide         8.0         mg/L           calculate Dissolved Oxygen Saturation for the facility's altitude at temp ctp [Idp = (14.62- (0.3898°ctp)+(0.006963°(ctp^2))-(0.00005897*(Ctp^3)))*(1-0.00000697*a)^5.167]         Idp         8.0         mg/L           calculate Initial Dissolved Oxygen Deficit for existing scenario [De=Ide-cde]         De         0.1         mg/L           calculate Initial Dissolved Oxygen Deficit for existing scenario [Dp=Idp-cdp]         Dp         0.2         mg/L           calculate Initial Dissolved Oxygen Deficit for existing scenario [It=(1/(k2e- k1e))*(log(((k2e/k1e)*(1-(De*(k2e-K1e)/(k1e*L0e)))))))         te         2.4         days           calculate time of travel to minimum DO of sag curve for proposed scenario [tp=(1/(k2e- k1e))*(log(((k2e/k1p)*(1-(De*(k2e-K1e)/(k1e*L0e)))))))         tp         2.4         days           calculate distance downstream to Minimum DO sag         calculate distance downstream to minimum DO sag proposed scenario [Me=(te*v*86400 seconds per day)/5280 feet per mile)]         miles           calculate distance downstream to minimum DO sag proposed scenario [Mp=(tp*v*86400 seconds per day)/5280 feet per mile)]         Mp         23.1         miles           calculate DO beficit at critical Time         calculate DO bef	57		L0p	6.0	
calculate Dissolved Oxygen Saturation for the facility's altitude at temp cte [Ide=(14.62- (0.3898*cte)+(0.006969*Cte^2))-(0.00005897*(Cte^3)))*(1-0.0000697*a)^5.167]         Ide         8.0         mg/L           calculate Dissolved Oxygen Saturation for the facility's altitude at temp ctp [Idp = (14.62- (0.3898*ctp)+(0.006969*(ctp^2))-(0.00005897*(ctp^3)))*(1-0.0000697*a)^5.167]         Idp         8.0         mg/L           62         calculate Initial Dissolved Oxygen Deficit for existing scenario [De=Ide-cde]         De         0.1         mg/L           63         calculate Initial Dissolved Oxygen Deficit for existing scenario [De=Idp-cdp]         Dp         0.2         mg/L           64         calculate time of Travel to Minimum DO Sag         Calculate time of travel to minimum DO of sag curve for existing scenario [te=(1/(k2e- k1e))*(log(((k2e/k1e)*(1-(De*(k2e-K1e)/(k1e*L0e))))))]         te         2.4         days           65         Calculate time of travel to minimum DO of sag curve for proposed scenario [tp=(1/(k2e- 6k t1e))*(log(((k2e/k1e)*(1-(De*(k2e-K1e)/(k1e*L0e))))))]         tp         2.4         days           68         calculate distance downstream to Minimum DO sag         existing scenario [Me=(te*v*86400 71 seconds per day)/5280 feet per mile)]         miles           73         Step 4 - Streeter-Phelps - Estimate Dissolved Oxygen Deficits at Critical Time 72         1.0         mg/L           74         Calculate DO deficit at critical time (tp) for proposed scenario [Ddp=((K1e*L0e)/(K2e-					
60         (0.3898*Cte)+(0.006969*Cte^2))-(0.00005897*(Cte^3)))*(1-0.0000697*a)^5.167]         Ide         8.0         mg/L           calculate Dissolved Oxygen Saturation for the facility's altitude at temp ctp [ldp = (14.62- 61 (0.3898*ctp)+(0.006969*(ctp^2))-(0.00005897*(ctp^3)))*(1-0.0000697*a)^5.167         Idp         8.0         mg/L           62         calculate Initial Dissolved Oxygen Deficit for existing scenario [De=lde-cde]         De         0.1         mg/L           63         calculate Initial Dissolved Oxygen Deficit for proposed scenario [De=lde-cde]         De         0.1         mg/L           64         Calculate Initial Dissolved Oxygen Deficit for proposed scenario [De=lde-cde]         De         0.1         mg/L           65         Calculate Time of Travel to Minimum DO Sag         E         E         2.4         days           64         Calculate time of travel to minimum DO of sag curve for proposed scenario [te=(1/(k2e- k1e))*(log(((k2e/k1e)*(1-(De*(k2e-K1e)/(k1e*L0e)))))))         te         2.4         days           67         K1p)*(log((k2e/k1e)*(1-(De*(k2e-K1e)/(k1e*L0e)))))))         tp         2.4         days           68         Calculate distance downstream to minimum DO sag proposed scenario [Me=(te*v*86400 seconds per day)/5280 feet per mile)]         Me         23.5         miles           72         Step 4 - Streeter-Phelps - Estimate Dissolved Oxygen Deficits at Critical Time calculate D	59				
61       (0.3898*ctp)+(0.006969*(ctp^2))-(0.00005897*(ctp^3))*(1-0.0000697*a)^5.167       Idp       8.0       mg/L         62       calculate Initial Dissolved Oxygen Deficit for existing scenario [De=Ide-cde]       De       0.1       mg/L         63       calculate Initial Dissolved Oxygen Deficit for proposed scenario [De=Idp-cdp]       Dp       0.2       mg/L         64	60	(0.3898*Cte)+(0.006969*Cte^2))-(0.00005897*(Cte^3)))*(1-0.00000697*a)^5.167]	Ide	8.0	mg/L
63       calculate Initial Dissolved Oxygen Deficit for proposed scenario [Dp=ldp-cdp]       Dp       0.2       mg/L         64              65       Calculate Time of Travel to Minimum DO Sag             64               65       Calculate Time of Travel to Minimum DO sag curve for existing scenario [te=(1/(k2e- 6k tte))*(log(((k2e/kte)*(1-(De*(k2e-K1e)/(k1e*L0e))))))]       te       2.4       days         67       ktp))*(log(((k2e/kte)*(1-(De*(k2e-K1e)/(k1e*L0e))))))]       tp       2.4       days         68		(0.3898*ctp)+(0.006969*(ctp^2))-(0.00005897*(ctp^3)))*(1-0.00000697*a)^5.167			•
64       Calculate Time of Travel to Minimum DO Sag       Calculate Time of Travel to Minimum DO of sag curve for existing scenario [te=(1/(k2e- k1e))*(log(((k2e/k1e)*(1-(De*(k2e-K1e)/(k1e*L0e))))))]       te       2.4       days         66       k1e)*(log(((k2e/k1e)*(1-(De*(k2e-K1e)/(k1e*L0e))))))]       te       2.4       days         67       k1e)*(log(((k2e/k1e)*(1-(De*(k2e-K1e)/(k1e*L0e))))))]       tp       2.4       days         67       k1p)*(log(((k2e/k1e)*(1-(De*(k2e-K1e)/(k1e*L0e))))))]       tp       2.4       days         68       Calculate Distance Downstream to Minimum DO sag curve for proposed scenario [Me=(te*v*86400       Me       23.5       miles         69       Calculate distance downstream to minimum DO sag proposed scenario [Mp=(tp*v*86400       Me       23.5       miles         70       seconds per day)/5280 feet per mile)]       Me       23.1       miles         72       73       Step 4 - Streeter-Phelps - Estimate Dissolved Oxygen Deficits at Critical Time       74       Calculate DO Deficit at Critical Time       75         74       Calculate DO deficit at critical time (te) for existing scenario [Dde=((K1e*L0e)/(K2e- 75 L1e))*(10^(-K1e*te)-10^(-K2e*te))+(De*10^(-K2e*te))]       Dde       1.0       mg/L         76       K1p)/*(10^(-K1e*te)-10^(-K2e*te))+(Dp*10^(-K2e*te))]       Dde       1.0       mg/L         77					Ŭ
65       Calculate Time of Travel to Minimum DO Sag			Ър	0.2	mg/∟
Calculate time of travel to minimum DO of sag curve for existing scenario [te=(1/(k2e-k1e)/(k1e)*(1-(De*(k2e-K1e)/(k1e*L0e)))))]te2.4daysCalculate time of travel to minimum DO of sag curve for proposed scenario [tp=(1/(k2p- k1p))*(log(((k2p/k1p)*(1-(Dp*(k2p-K1p)/(k1p*L0p)))))])tp2.4days67k1p))*(log((((k2p/k1p)*(1-(Dp*(k2p-K1p)/(k1p*L0p))))))]tp2.4days68calculate Distance Downstream to Minimum DO sag calculate distance downstream to minimum DO sag existing scenario [Me=(te*v*86400 seconds per day)/5280 feet per mile)]Me23.570seconds per day)/5280 feet per mile)]Me23.1miles72seconds per day)/5280 feet per mile)]Mp23.1miles73Step 4 - Streeter-Phelps - Estimate Dissolved Oxygen Deficits at Critical Time calculate DO deficit at critical time (te) for existing scenario [Dde=((k1e*L0e)/(K2e- T5 L1e))*(10^{-(-K1e*te)-10^{-(-K2e*te))})Dde1.0mg/L74Calculate DO deficit at critical time (tp) for proposed scenario [Ddp=((K1p*L0p)/(C48- K1p))*(10^{-(-K1p*tp)-10^{-(-K2p*tp))+(Dp*10^{-(-K2e*te))})Dde1.1mg/L777770707070707078Calculate Minimum DOscenario [DOe=Ide-Dde]DOe7.00mg/L		Calculate Time of Travel to Minimum DO Sag			
Calculate time of travel to minimum DO of sag curve for proposed scenario [tp=(1/(k2p- k1p))*(log(((k2p/k1p)*(1-(Dp*(k2p-K1p)/(k1p*L0p))))))]       tp       2.4       days         68       69       Calculate Distance Downstream to Minimum DO Sag           69       Calculate distance downstream to minimum DO sag existing scenario [Me=(te*v*86400       Me       23.5       miles         70       seconds per day)/5280 feet per mile)]       Me       23.5       miles         71       seconds per day)/5280 feet per mile)]       Mp       23.1       miles         72       72       72       72       72         73       Step 4 - Streeter-Phelps - Estimate Dissolved Oxygen Deficits at Critical Time       74       74         74       Calculate DO deficit at Critical Time       74       74         75       L1e))*(10^(-K1e*te)-10^(-K2e*te))+(De*10^(-K2e*te))]       Dde       1.0       mg/L         76       K1p))*(10^{(-K1p*tp)-10^{(-K2p*tp))+(Dp*10^{(-K2p*tp))})       Ddp       1.1       mg/L         77       77       74       74       74       74       74       74         75       L1e))*(10^{(-K1p*tp)-10^{(-K2p*tp))+(De*10^{(-K2e*te))]       Dde       1.0       mg/L         76       K1p))*(10^{(1/(-K1p*tp)-10^{(-k2p*tp))+(Dp*10^{(-k2p*tp))}) <td></td> <td>Calculate time of travel to minimum DO of sag curve for existing scenario [te=(1/(k2e-</td> <td></td> <td></td> <td></td>		Calculate time of travel to minimum DO of sag curve for existing scenario [te=(1/(k2e-			
67       k1p))*(log(((k2p/k1p)*(1-(Dp*(k2p-K1p)/(k1p*L0p))))))       tp       2.4       days         68       68       68       68       68       69       60 <t< td=""><td>66</td><td></td><td>te</td><td>2.4</td><td>days</td></t<>	66		te	2.4	days
68       100 Calculate Distance Downstream to Minimum DO Sag       100 Calculate Distance Downstream to minimum DO sag existing scenario [Me=(te*v*86400         70       seconds per day)/5280 feet per mile)]       Me       23.5         71       seconds per day)/5280 feet per mile)]       Me       23.1         72       Mp       23.1       miles         73       Step 4 - Streeter-Phelps - Estimate Dissolved Oxygen Deficits at Critical Time       72         73       Step 4 - Streeter-Phelps - Estimate Dissolved Oxygen Deficits at Critical Time       74         74       Calculate DO Deficit at Critical Time       1.0         75       L1e))*(10^{(-K1e*te)-10^{(-K2e*te))+(De*10^{(-K2e*te))]}       Dde       1.0         75       calculate DO deficit at critical time (tp) for proposed scenario [Ddp=((K1p*L0p)/(C48- K1p))*(10^{(-K1p*tp)-10^{(-k2p*tp))+(Dp*10^{(-k2p*tp))})       Ddp       1.1         76       Calculate Minimum DO       77       78       Calculate Minimum DO         77       78       Calculate Minimum DO, existing scenario [DOe=Ide-Dde]       DOe       7.00       mg/L	67		tn	24	davs
calculate distance downstream to minimum DO sag existing scenario [Me=(te*v*86400 seconds per day)/5280 feet per mile)]Me23.5milescalculate distance downstream to minimum DO sag proposed scenario [Mp=(tp*v*86400 seconds per day)/5280 feet per mile)]Mp23.1miles72727273Step 4 - Streeter-Phelps - Estimate Dissolved Oxygen Deficits at Critical Time74Calculate DO Deficit at Critical Time7474Calculate DO deficit at critical time (te) for existing scenario [Dde=((k1e*L0e)/(K2e- L1e))*(10^(-K1e*te)-10^(-K2e*te))+(De*10^(-K2e*te))]Dde1.0mg/L76K1p))*(10^(-K1p*tp)-10^(-k2p*tp))+(Dp*10^(-k2p*tp))Ddp1.1mg/L7778Calculate Minimum DO23.0mg/L70.0mg/L			ιp	2.7	uays
70seconds per day)/5280 feet per mile)]Me23.5milescalculate distance downstream to minimum DO sag proposed scenario [Mp=(tp*v*86400Mp23.1miles71seconds per day)/5280 feet per mile)]Mp23.1miles7273Step 4 - Streeter-Phelps - Estimate Dissolved Oxygen Deficits at Critical Time74Calculate DO Deficit at Critical Time74Calculate DO deficit at critical time (te) for existing scenario [Dde=((k1e*L0e)/(K2e- C L1e))*(10^(-K1e*te)-10^(-K2e*te))+(De*10^(-K2e*te))]Dde1.0mg/L75L1e))*(10^(-K1p*tp)-10^(-k2p*tp))+(Dp*10^(-k2p*tp)))Ddp1.1mg/L77777778Calculate Minimum DO, existing scenario [DOe=lde-Dde]DOe7.00mg/L		Calculate Distance Downstream to Minimum DO Sag			
calculate distance downstream to minimum DO sag proposed scenario [Mp=(tp*v*86400       Mp       23.1       miles         71       seconds per day)/5280 feet per mile)]       Mp       23.1       miles         72       73       Step 4 - Streeter-Phelps - Estimate Dissolved Oxygen Deficits at Critical Time       74         74       Calculate DO Deficit at Critical Time       74       Calculate DO deficit at critical time (te) for existing scenario [Dde=((k1e*L0e)/(K2e-       75         75       L1e))*(10^(-K1e*te)-10^(-K2e*te))+(De*10^(-K2e*te))]       Dde       1.0       mg/L         76       K1p))*(10^(-K1p*tp)-10^(-k2p*tp))+(Dp*10^(-k2p*tp))       Ddp       1.1       mg/L         77       74       76       76       77       77         77       77       70       70       70         78       Calculate Minimum DO       70       700       mg/L					
71seconds per day)/5280 feet per mile)]Mp23.1miles7273Step 4 - Streeter-Phelps - Estimate Dissolved Oxygen Deficits at Critical Time1174Calculate DO Deficit at Critical Time11calculate DO deficit at critical time (te) for existing scenario [Dde=((k1e*L0e)/(K2e- L1e))*(10^(-K1e*te)-10^(-K2e*te))+(De*10^(-K2e*te))]Dde1.0mg/Lcalculate DO deficit at critical time (tp) for proposed scenario [Ddp=((K1p*L0p)/(C48- K1p))*(10^(-K1p*tp)-10^(-k2p*tp))+(Dp*10^(-k2p*tp)))Ddp1.1mg/L76Calculate Minimum DO11mg/L78Calculate Minimum DO, existing scenario [DOe=lde-Dde]DOe7.00mg/L	70		Me	23.5	miles
72       72         73       Step 4 - Streeter-Phelps - Estimate Dissolved Oxygen Deficits at Critical Time         74       Calculate DO Deficit at Critical Time         calculate DO deficit at critical time (te) for existing scenario [Dde=((k1e*L0e)/(K2e-         75       L1e))*(10^(-K1e*te)-10^(-K2e*te))+(De*10^(-K2e*te))]         calculate DO deficit at critical time (tp) for proposed scenario [Ddp=((K1p*L0p)/(C48-         76       K1p))*(10^(-K1p*tp)-10^(-k2p*tp))+(Dp*10^(-k2p*tp))         77       77         78       Calculate Minimum DO         79       calculate minimum DO, existing scenario [DOe=lde-Dde]	71		Мр	23.1	miles
74       Calculate DO Deficit at Critical Time       Image: Calculate DO deficit at critical time (te) for existing scenario [Dde=((k1e*L0e)/(K2e-         75       L1e))*(10^(-K1e*te)-10^(-K2e*te))+(De*10^(-K2e*te))]       Dde       1.0       mg/L         calculate DO deficit at critical time (tp) for proposed scenario [Ddp=((K1p*L0p)/(C48-       Image: Calculate DO deficit at critical time (tp) for proposed scenario [Ddp=((K1p*L0p)/(C48-       Image: Calculate Dop deficit at critical time (tp) for proposed scenario [Ddp=((K1p*L0p)/(C48-         76       K1p))*(10^(-K1p*tp)-10^(-k2p*tp))+(Dp*10^(-k2p*tp))       Ddp       1.1       mg/L         77       Image: Calculate Minimum DO       Image: Calculate Minimum DO       Image: Calculate Minimum DO       Image: Calculate Minimum DO         79       calculate minimum DO, existing scenario [DOe=Ide-Dde]       DOe       7.00       mg/L					
calculate DO deficit at critical time (te) for existing scenario [Dde=((k1e*L0e)/(K2e- Dde 1.0 mg/L75L1e))*(10^(-K1e*te)-10^(-K2e*te))+(De*10^(-K2e*te))]Dde 1.0 mg/Lcalculate DO deficit at critical time (tp) for proposed scenario [Ddp=((K1p*L0p)/(C48- T6 K1p))*(10^(-K1p*tp)-10^(-k2p*tp))+(Dp*10^(-k2p*tp))Ddp 1.1 mg/L77777878Calculate Minimum DO ralculate minimum DO, existing scenario [DOe=lde-Dde]DOe 7.00 mg/L	73				
75       L1e))*(10^(-K1e*te)-10^(-K2e*te))+(De*10^(-K2e*te))]       Dde       1.0       mg/L         calculate DO deficit at critical time (tp) for proposed scenario [Ddp=((K1p*L0p)/(C48-       Ddp       1.1       mg/L         76       K1p))*(10^(-K1p*tp)-10^(-k2p*tp))+(Dp*10^(-k2p*tp))       Ddp       1.1       mg/L         77       77       78       Calculate Minimum DO       79       calculate minimum DO, existing scenario [DOe=lde-Dde]       DOe       7.00       mg/L	74				
76       K1p))*(10^(-K1p*tp)-10^(-k2p*tp))+(Dp*10^(-k2p*tp))       Ddp       1.1       mg/L         77	75	L1e))*(10^(-K1e*te)-10^(-K2e*te))+(De*10^(-K2e*te))]	Dde	1.0	mg/L
78       Calculate Minimum DO         79       calculate minimum DO, existing scenario [DOe=lde-Dde]         DOe       7.00         mg/L			Ddp	1.1	mg/L
79 calculate minimum DO, existing scenario [DOe=lde-Dde]    DOe    7.00    mg/L		Coloulata Minimum DO			
			DOe	7.00	ma/l
			DOe	6.91	mg/L

	А	В	С	D				
81								
82	WARNING #1							
	If min. D.O. (DOe) is < water quality criterion, model is predicting a water quality impairment under <b>existing</b> conditions, no assimilative capacity is present, If D.O. is > or = criterion proceed with model.	Proceed with model						
84	WARNING #2							
	If min. D.O. (DOp) is < water quality criterion, model is predicting a water quality impairment under proposed conditions, no assimilative capacity is present, If D.O. is > or = criterion proceed with model.	Proceed with model						
	Step 5 - Determine Available Pollutant Assimilative Capacity with the Discharge at Ex	isting &	Proposed D	esign				
	Flows calculate the change in minimum DO resulting from the proposed discharge, [DOc=DOe- DOp]	DOp	0.10	mg/L				
88 89	calculate remaining assimilative capacity, (existing scenario) [ACe=-(WQ-DOe)]	ACe	2.00	mg/L				
90	Step 6 - Determine if proposed new or added discharge is <i>de minimis</i> or if a full antidegradation review will be required. Antideg review is required if the new discharge will consume greater than 10% of the remaining assimilative capacity. Discharges that consume 10% or less of the remaining assimilative capacity will be considered " <i>de minimis</i> " and do not require a full antidegradation review.							
91	calculate 10% of remaining assimilative capacity, [Ar=ACe*0.1]	Ar	0.200	mg/L				
92 93	Determine if Antideg review is required or if new discharge is <i>de</i> " <i>minimis</i> "		de mir	nimis				
94	If DOp > Ar then Antideg review required, if DOp < or = Ar then the discharge is de minimis							

				cted to Elevation		ty	
Prepa	red by NMED-	SWQB using	references fro	om USGS-WR	D Colo. Dist.		
<b>Instructions:</b> Enter Information on Local Water Quality Conditions in Yellow Boxes on the "Assimilative Capacity - BOD" worksheet of this workbook. Blue shaded boxes will automatically calculate.		Temperature (deg C)	Elevation above Sea Level (feet)	Specific Conductance (uS/cm)	corrected to	Dxygen Solubility o local Elevation d Salinity	
	Scenario 1 (existing)	17.1	5000	500	8.0	mg/l	
	Scenario 2 (proposed)	17.1	5000	500	8.0	mg/l	
Intermediate Operations	Value Scenario 1	Value Scenario 2			Formula		
Calculate Salinity in 0/00 using Specific Conductance (Salinity)	0.28	0.28	Salinity=((0.0005572*Conductivity)+(0.0000000202*(Conductivity^2)))				
Calculate natural log of DO Solubility at sea level in ml/l using salinity derived above (InDO)	1.91	1.91	InDO = - 173.4292+249.6339*(100/(273.15+Temp))+143.3483*LN((273.15+Temp)/ 100)-21.8492*((Temp+273.15)/100)+Salinity*(- 0.033096+0.014259*((Temp+273.15)/100)- 0.0017*((Temp+273.15)/100)^2)				
Calculate the DO (ml/l) from the natural log of DO (DOml)	6.73	6.73	DOml=EXP(InDO)				
Convert DO ml/l to mg/l (DOmg)	9.61	9.61	DOmg=DOml*1.4276				
Calculate log of vapor pressure in mm Hg (log_v_press)	1.16	1.16	log_v_press=8.10765-(1750.286/(235+Temp))				
Calculate vapor pressure from log_v_press (vapor pressure)	14.58	14.59	vap_press=10^log_v_press				
Calculate D.O. Solubility (mg/l) at local altitude and specific conductance (DO')	8.0	8.0	DO'=DOmg*(((760-2.5*(Elevation/100))-vapor_press)/(760-vapor_press))				